



Vermont Agency of Transportation  
I-91  
Windsor County  
Project Number: IM 091-2(79)

Hartford Lateral Slide

**Contractor-Fabricated Pre-Cast Concrete Structures:**

**Approach Slabs**

Prepared By,

Erich Heymann

May 26, 2015

**PCL Civil Constructors Inc.**

3810 Northdale Blvd. Suite 200

Tampa, Florida 33624

813-264-9500

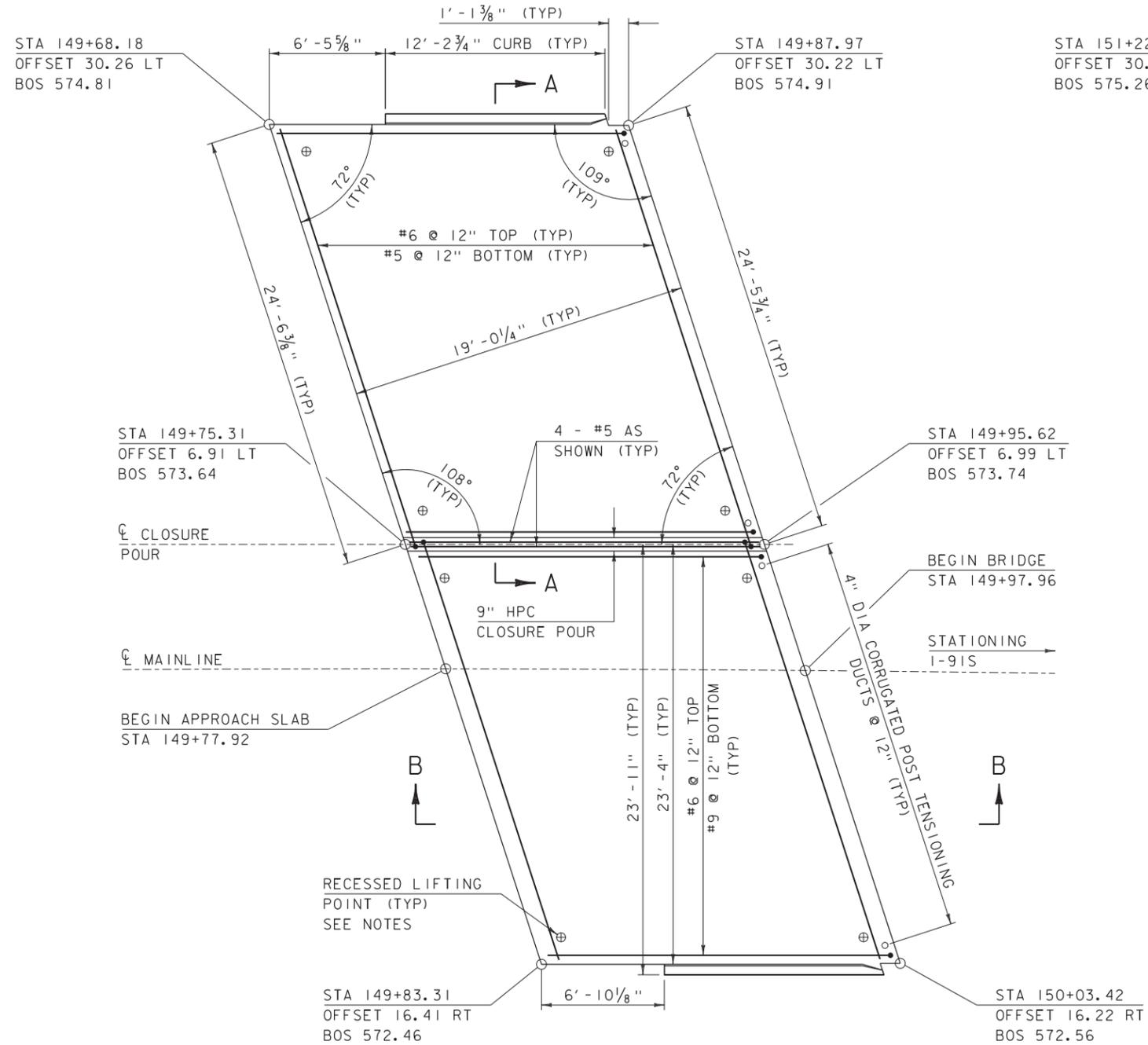
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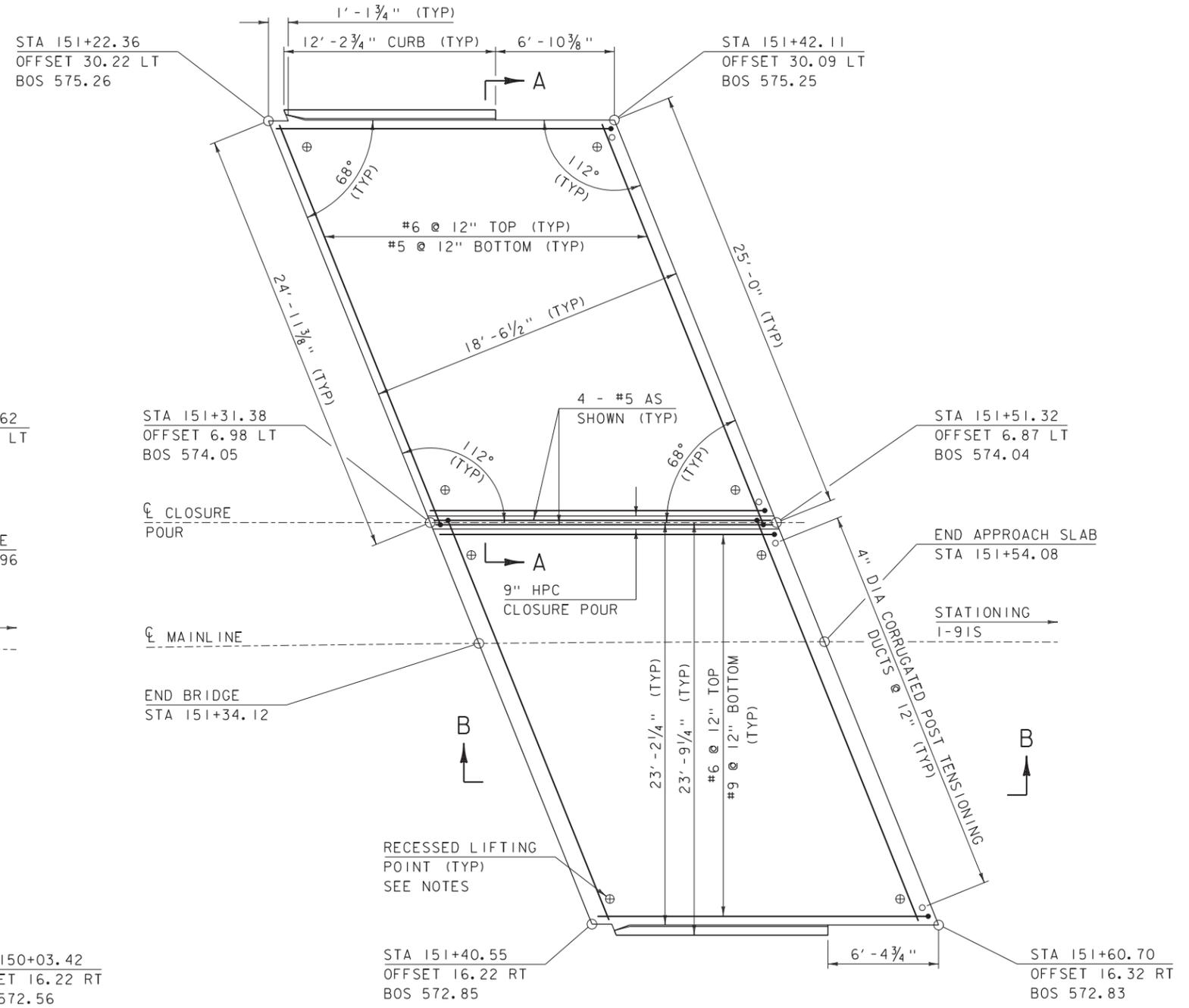
## REFERENCED SUBMITTALS

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**FABRICATION DRAWINGS  
(ORIGINAL CONTRACT  
DRAWINGS)**



**APPROACH SLAB 1 PLAN**  
SCALE 1/4" = 1'-0"

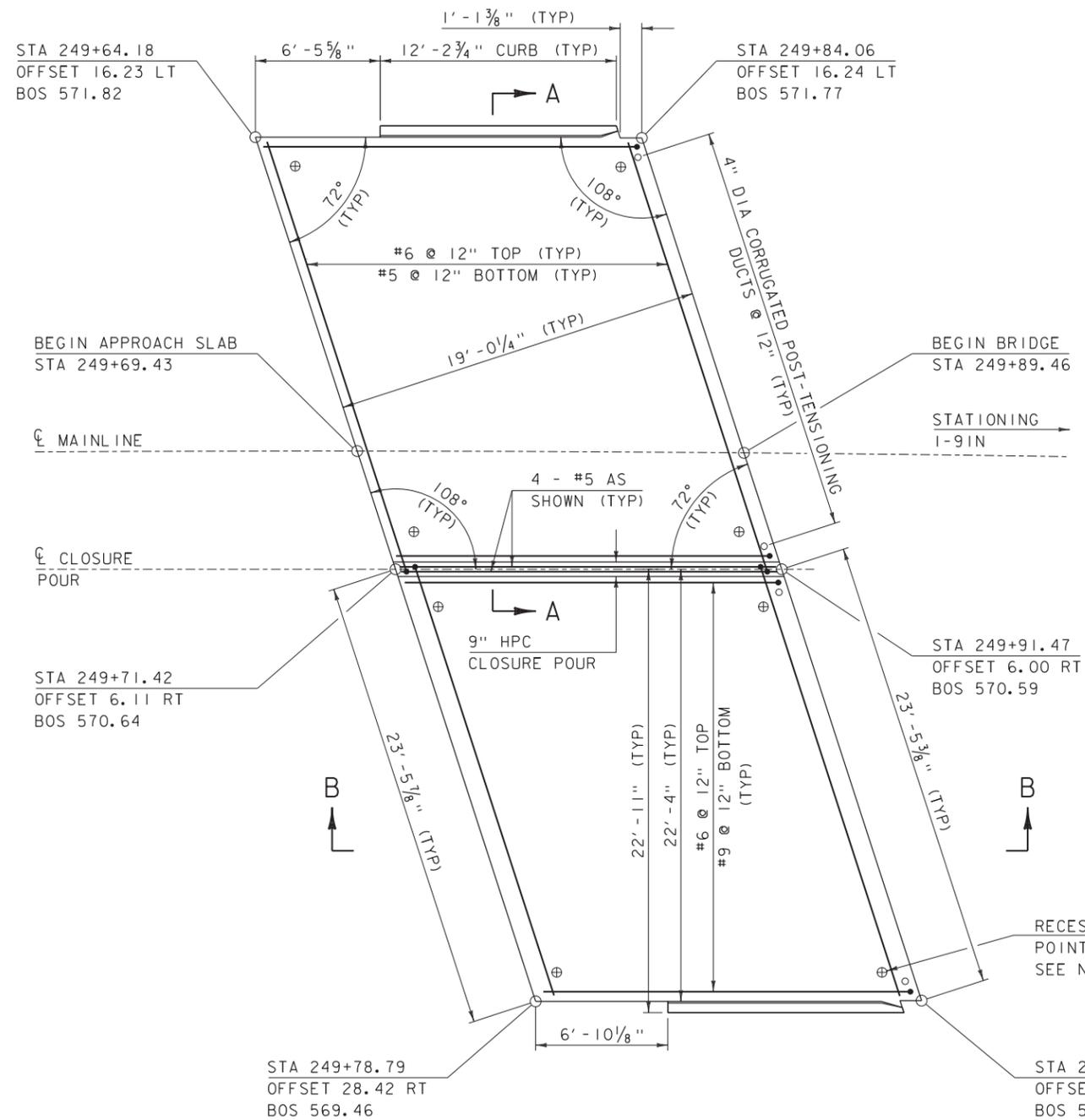


**APPROACH SLAB 2 PLAN**  
SCALE 1/4" = 1'-0"

- NOTES:**
- 1) ALL APPROACH SLAB REINFORCING STEEL SHALL BE LEVEL II OR HIGHER.
  - 2) BOS = BOTTOM OF SLAB
  - 3) LIFTING POINTS SHALL BE DESIGNED BY OTHERS AND CALCULATIONS INCLUDED WITH SUBMITTAL.

- NOTE:**
- NF = NEAR FACE
  - FF = FAR FACE
  - EF = EACH FACE
  - 3" CLEAR, UNLESS OTHERWISE SPECIFIED ON THE PLANS.
  - 2'-2" BAR LAP UNLESS OTHERWISE SPECIFIED ON THE PLANS.

PROJECT NAME: HARTFORD	
PROJECT NUMBER: IM 091-2(79)	
FILE NAME: sl2al32apslabs_43S.dgn	PLOT DATE: 15-DEC-2014
PROJECT LEADER: K. HIGGINS	DRAWN BY: K. FRIEDLAND
DESIGNED BY: G. LAROCHE	CHECKED BY: W. LAMMER
APPROACH SLAB DETAILS 43S	SHEET 97 OF 166

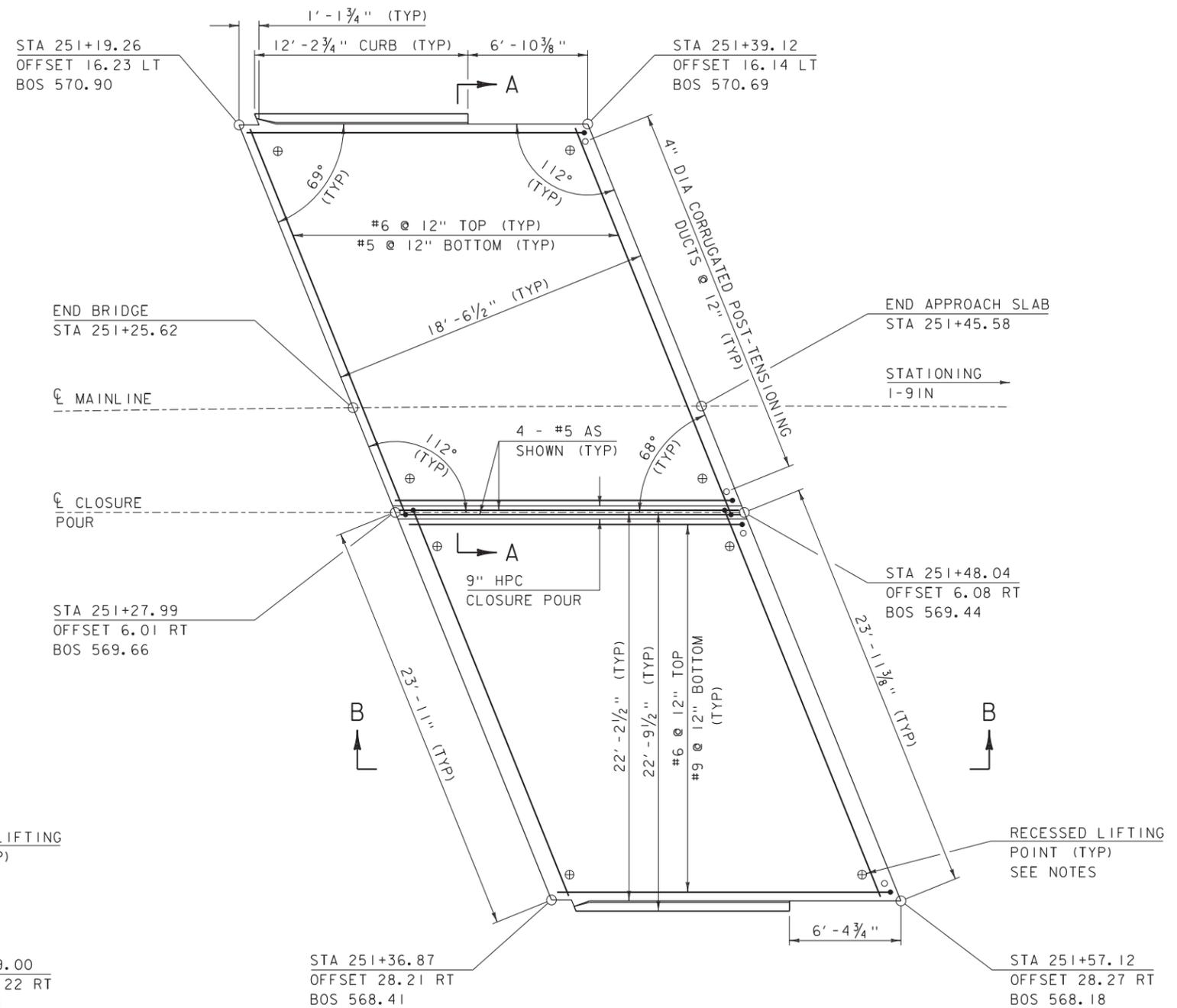


APPROACH SLAB 3 PLAN

SCALE 1/4" = 1'-0"

NOTES:

- 1) ALL APPROACH SLAB REINFORCING STEEL SHALL BE LEVEL II OR HIGHER.
- 2) BOS = BOTTOM OF SLAB
- 3) LIFTING POINTS SHALL BE DESIGNED BY OTHERS AND CALCULATIONS INCLUDED WITH SUBMITTAL.



APPROACH SLAB 4 PLAN

SCALE 1/4" = 1'-0"

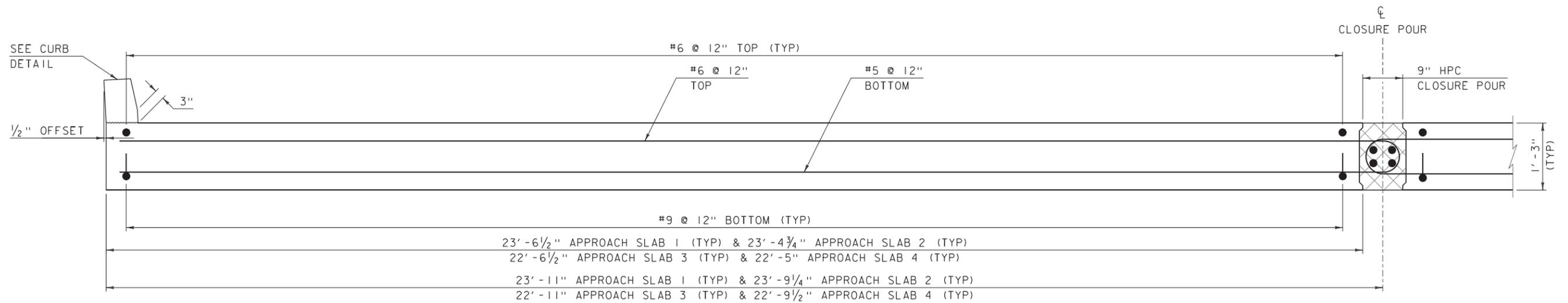
NOTE:

- NF = NEAR FACE
- FF = FAR FACE
- EF = EACH FACE
- 3" CLEAR, UNLESS OTHERWISE SPECIFIED ON THE PLANS.
- 2'-2" BAR LAP UNLESS OTHERWISE SPECIFIED ON THE PLANS.

PROJECT NAME: HARTFORD  
 PROJECT NUMBER: IM 091-2(79)

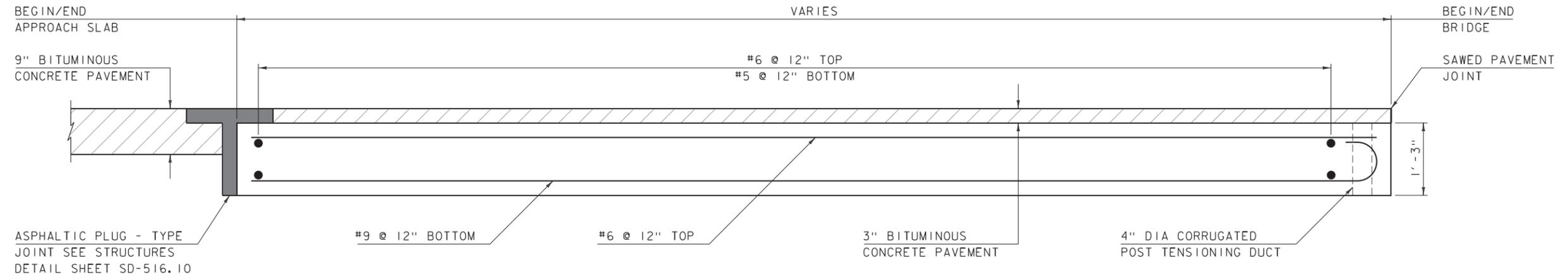
FILE NAME: sl2al32apslabs\_43N.dgn  
 PROJECT LEADER: K. HIGGINS  
 DESIGNED BY: G. LAROCHE  
 APPROACH SLAB DETAILS 43N

PLOT DATE: 15-DEC-2014  
 DRAWN BY: K. FRIEDLAND  
 CHECKED BY: W. LAMMER  
 SHEET 98 OF 166



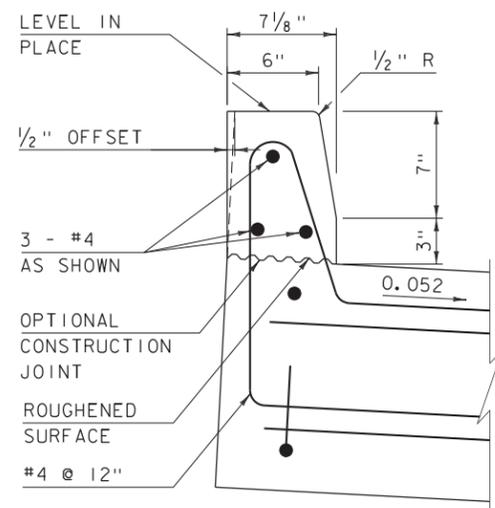
**SECTION A-A**

SCALE 1" = 1'-0"



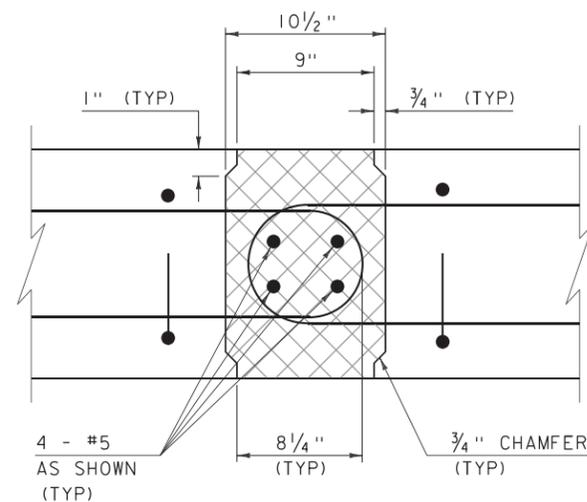
**SECTION B-B**

SCALE 1" = 1'-0"



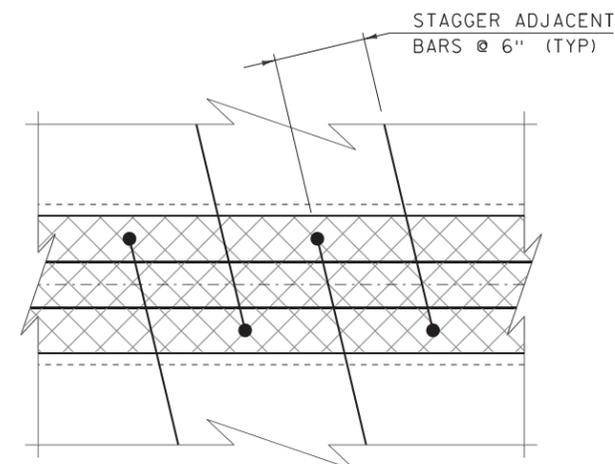
**CURB DETAIL**

SCALE 2" = 1'-0"



**JOINT DETAIL SECTION**

SCALE 2" = 1'-0"



**JOINT DETAIL PLAN**

SCALE 2" = 1'-0"

**NOTE:**

NF = NEAR FACE  
FF = FAR FACE  
EF = EACH FACE  
▲ = CUT TO FIT IN FIELD  
3" CLEAR, UNLESS OTHERWISE  
SPECIFIED ON THE PLANS.  
2'-2" BAR LAP UNLESS OTHERWISE  
SPECIFIED ON THE PLANS.

**NOTES:**

1) ALL APPROACH SLAB REINFORCING STEEL SHALL  
BE LEVEL II OR HIGHER.

PROJECT NAME: HARTFORD  
PROJECT NUMBER: IM 091-2(79)

FILE NAME: sl2al32apslabs\_435.dgn  
PROJECT LEADER: K. HIGGINS  
DESIGNED BY: G. LAROCHE  
APPROACH SLAB DETAILS

PLOT DATE: 15-DEC-2014  
DRAWN BY: K. FRIEDLAND  
CHECKED BY: W. LAMMER  
SHEET 99 OF 166

# **DESIGN & ANALYSIS OF LIFTING ATTACHMENTS**



Vermont Agency of Transportation  
I-91  
Windsor County  
Project Number: IM 091-2(79)

## Hartford Lateral Slide

Calculations for Temporary Structures including:

Approach Slab Lifting Attachments

Submitted By,

Tim Davis, P.E.  
VT P.E. 97183

Erich Heymann, E.I.  
E.I. #1100014027



May 7 2015 8:39 AM



May 5, 2015

**PCL Civil Constructors Inc.**

3810 Northdale Blvd. Suite 200  
Tampa, Florida 33624  
813-264-9500



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Job No	Sheet No <b>1</b>	Rev
Part		
Ref		
By	Date 10-Nov-14	Chd
Client	File Hartford Approach.std	Date/Time 30-Apr-2015 16:04

## Job Information

	Engineer	Checked	Approved
Name:			
Date:	10-Nov-14		

Structure Type	SPACE FRAME
----------------	-------------

Number of Nodes	529	Highest Node	1009
Number of Elements	15	Highest Beam	498
Number of Plates	475	Highest Plate	475

Number of Basic Load Cases	1
Number of Combination Load Cases	0

Included in this printout are data for:

All	The Whole Structure
-----	---------------------

Included in this printout are results for load cases:

Type	L/C	Name
Primary	1	LOAD CASE 1

## Section Properties

Prop	Section	Area (in <sup>2</sup> )	I <sub>yy</sub> (in <sup>4</sup> )	I <sub>zz</sub> (in <sup>4</sup> )	J (in <sup>4</sup> )	Material
2	Cir 0.96	0.724	0.042	0.042	0.083	STEEL
3	PIPS60	5.220	26.500	26.500	52.924	STEEL
4	Cir 1.00	0.785	0.049	0.049	0.098	STEEL

## Plate Thickness

Prop	Node A (in)	Node B (in)	Node C (in)	Node D (in)	Material
1	15.000	15.000	15.000	15.000	CONCRETE

## Selfweight : 1 LOAD CASE 1

Direction	Factor
Y	-1.000



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Job No	Sheet No <b>2</b>	Rev
Part		
Ref		
By		Date 10-Nov-14 Chd
Client	File Hartford Approach.std	Date/Time 30-Apr-2015 16:04

## Beam Maximum Forces by Section Property

Section		Axial	Shear		Torsion	Bending	
		Max Fx (kip)	Max Fy (kip)	Max Fz (kip)	Max Mx (kip'in)	Max My (kip'in)	Max Mz (kip'in)
Cir 0.96	Max +ve		0.013	0.000	0.008	0.022	0.683
	Max -ve	-51.844	-0.014	-0.000	-0.006	-0.029	-0.322
PIPS60	Max +ve	25.274	0.198		0.007	0.007	
	Max -ve		-0.198	-0.000	-0.003	-0.007	-13.787
Cir 1.00	Max +ve		0.000	0.000	0.000	0.021	0.025
	Max -ve	-22.342	-0.000	-0.000	-0.000	-0.021	-0.025

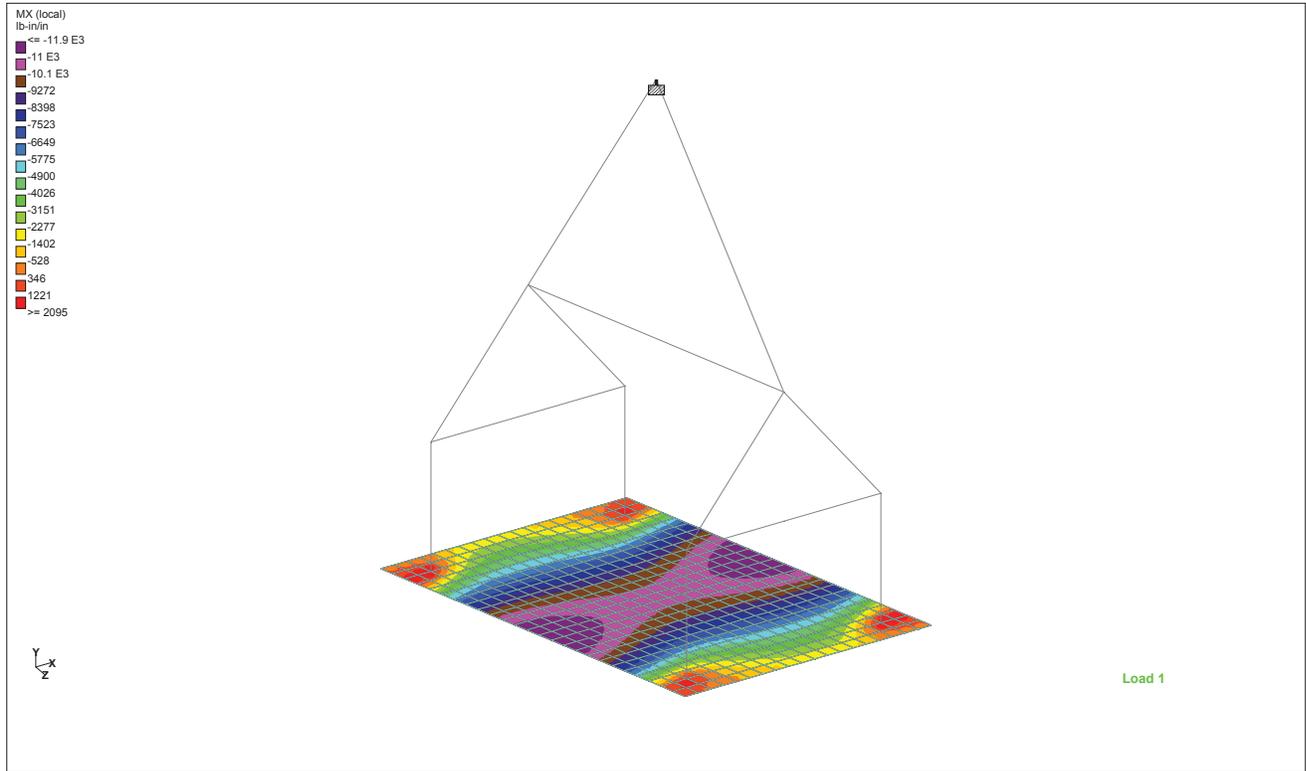
## Reaction Summary

	Node	L/C	Horizontal	Vertical	Horizontal	Moment		
			FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
Max FX	1001	1:LOAD CASE	<b>-0.000</b>	90.532	-0.000	-0.000	-0.000	-0.001
Min FX	1001	1:LOAD CASE	<b>-0.000</b>	90.532	-0.000	-0.000	-0.000	-0.001
Max FY	1001	1:LOAD CASE	-0.000	<b>90.532</b>	-0.000	-0.000	-0.000	-0.001
Min FY	1001	1:LOAD CASE	-0.000	<b>90.532</b>	-0.000	-0.000	-0.000	-0.001
Max FZ	1001	1:LOAD CASE	-0.000	90.532	<b>-0.000</b>	-0.000	-0.000	-0.001
Min FZ	1001	1:LOAD CASE	-0.000	90.532	<b>-0.000</b>	-0.000	-0.000	-0.001
Max MX	1001	1:LOAD CASE	-0.000	90.532	-0.000	<b>-0.000</b>	-0.000	-0.001
Min MX	1001	1:LOAD CASE	-0.000	90.532	-0.000	<b>-0.000</b>	-0.000	-0.001
Max MY	1001	1:LOAD CASE	-0.000	90.532	-0.000	-0.000	<b>-0.000</b>	-0.001
Min MY	1001	1:LOAD CASE	-0.000	90.532	-0.000	-0.000	<b>-0.000</b>	-0.001
Max MZ	1001	1:LOAD CASE	-0.000	90.532	-0.000	-0.000	-0.000	<b>-0.001</b>
Min MZ	1001	1:LOAD CASE	-0.000	90.532	-0.000	-0.000	-0.000	<b>-0.001</b>



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Job No	Sheet No <b>3</b>	Rev
Part		
Ref		
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Local X Moment

Max Moment = 11.9 k-ft/ft, requires # 9 bars at 26" OC (see next sheet).  
 #9's provided at 12" O.C. so OK

Overall Shear = 45 kips / (18' x 1.25') = 2 ksf = 13 psi <  $2\sqrt{f'c}$  -----> OK



Project No: \_\_\_\_\_

By: TMD

Date: 4/30/2015

Project: \_\_\_\_\_

Checked By: \_\_\_\_\_

Date: \_\_\_\_\_

### Calculation Of Required Reinforcing Rebars

Subject: \_\_\_\_\_

Calculation For: \_\_\_\_\_

#### Input

M (DL)=	11.9 FT.KIPS	Factor DL=	1.5
M (LL)=	FT.KIPS	Factor LL=	1
Mu=	FT.KIPS	f'c=	5 KSI
d=	12 IN	fy=	60 KSI
b=	12 IN	As(prov)=	0 IN <sup>2</sup>

#### Output

Moment (Mu)=	17.9 FT.KIPS	X=	20.06391
A=	31.76	Y=	0.336093
B=	-648.0		
C=	214.2		
Δ=	392688		
β <sub>1</sub> =	0.80 ACI (10.2.7.3)	(A) As <sup>2</sup> +(B) As + (C) =0	
ρ Min=	0.0035 ACI (10.5.1)	As=	0.336093 IN <sup>2</sup>
ρ Max=	0.0252 ACI (10.3.3)	a=	0.40 IN
ρ Actual=	0.0023	Cc=	20 KIPS
Required As=	0.34 IN <sup>2</sup>	T=	20 KIPS
Min As=	0.51 IN <sup>2</sup>	<b>Use the minimum of 1.33 Req'd As or As min</b>	
Max As=	3.62 IN <sup>2</sup>	φMn=	0.0 FT.KIPS

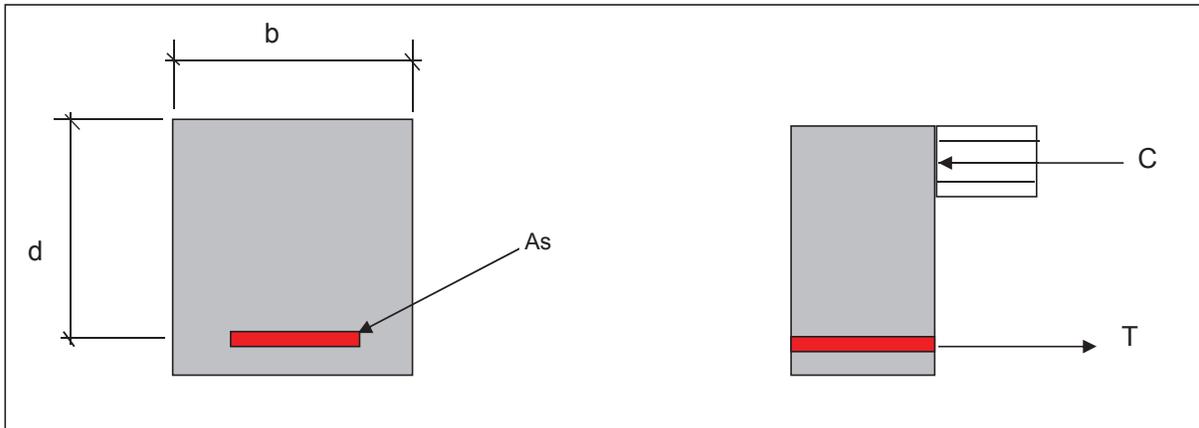
Final As (IN<sup>2</sup>)= **0.45**

% of ρ Max= **12.3412 %**

Bar Selection:

5	#3	0.55
3	#4	0.60
2	#5	0.62
2	#6	0.88
1	#7	0.60
1	#8	0.79
1	#9	1.00
1	#10	1.27
1	#11	1.56

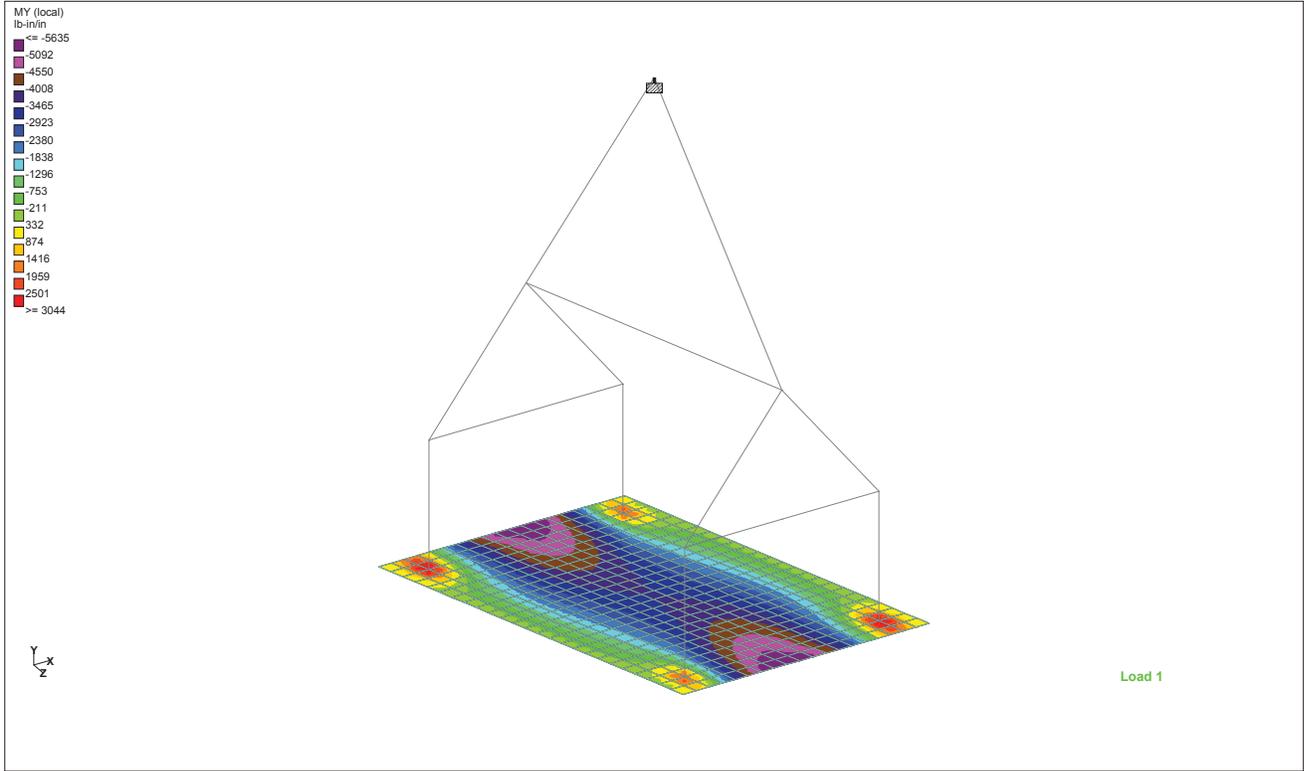
or	#3 @	2.95 o.c.
or	#4 @	5.37 o.c.
or	#5 @	8.32 o.c.
or	#6 @	11.81 o.c.
or	#7 @	16.11 o.c.
or	#8 @	21.21 o.c.
or	#9 @	26.85 o.c.
or	#10 @	34.09 o.c.
or	#11 @	41.88 o.c.





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Job No	Sheet No <b>4</b>	Rev
Part		
Ref		
By	Date 10-Nov-14	Chd
Client	File Hartford Approach.std	Date/Time 30-Apr-2015 16:04



Local Y Moment

Max Moment = 5.6 k-ft/ft, requires # 5 bars at 16" OC (see next sheet). #5's provided at 12" O.C. so OK



Project No: \_\_\_\_\_

By: TMD

Date: 4/30/2015

Project: \_\_\_\_\_

Checked By: \_\_\_\_\_

Date: \_\_\_\_\_

### Calculation Of Required Reinforcing Rebars

Subject: \_\_\_\_\_

Calculation For: \_\_\_\_\_

#### Input

M (DL)=	5.63 FT.KIPS	Factor DL=	1.5
M (LL)=	FT.KIPS	Factor LL=	1
Mu=	FT.KIPS	f'c=	5 KSI
d=	11 IN	fy=	60 KSI
b=	12 IN	As(prov)=	0 IN <sup>2</sup>

#### Output

Moment (Mu)=	8.4 FT.KIPS	X=	18.52781
A=	31.76	Y=	0.172192
B=	-594.0		
C=	101.3		
Δ=	339960		
β <sub>1</sub> =	0.80 ACI (10.2.7.3)	(A) As <sup>2</sup> +(B) As + (C) =0	
ρ Min=	0.0035 ACI (10.5.1)	As=	0.172192 IN <sup>2</sup>
ρ Max=	0.0252 ACI (10.3.3)	a=	0.20 IN
ρ Actual=	0.0013	Cc=	10 KIPS
Required As=	0.17 IN <sup>2</sup>	T=	10 KIPS
Min As=	0.47 IN <sup>2</sup>	<b>Use the minimum of 1.33 Req'd As or As min</b>	
Max As=	3.32 IN <sup>2</sup>	φMn=	0.0 FT.KIPS

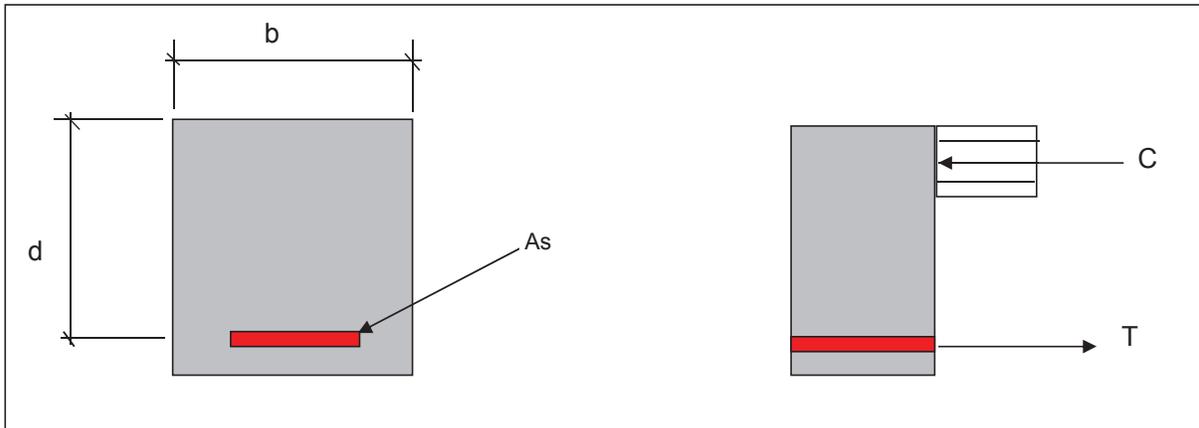
Final As (IN<sup>2</sup>)= **0.23**

% of ρ Max= **6.89761** %

Bar Selection:

3	#3	0.33
2	#4	0.40
1	#5	0.31
1	#6	0.44
1	#7	0.60
1	#8	0.79
1	#9	1.00
1	#10	1.27
1	#11	1.56

or	#3 @	5.76 o.c.
or	#4 @	10.48 o.c.
or	#5 @	16.24 o.c.
or	#6 @	23.06 o.c.
or	#7 @	31.44 o.c.
or	#8 @	41.39 o.c.
or	#9 @	52.40 o.c.
or	#10 @	66.55 o.c.
or	#11 @	81.74 o.c.





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Job No	Sheet No <b>1</b>	Rev
Part		
Ref		
By	Date 10-Nov-14	Chd
Client	File Hartford Approach.std	Date/Time 28-Apr-2015 13:04

### approach slab rigging and punching shear

each support point - 22.3 kips

pullout perimeter =  $10+10+6+6 = 32"$   
Pullout depth = 6" min

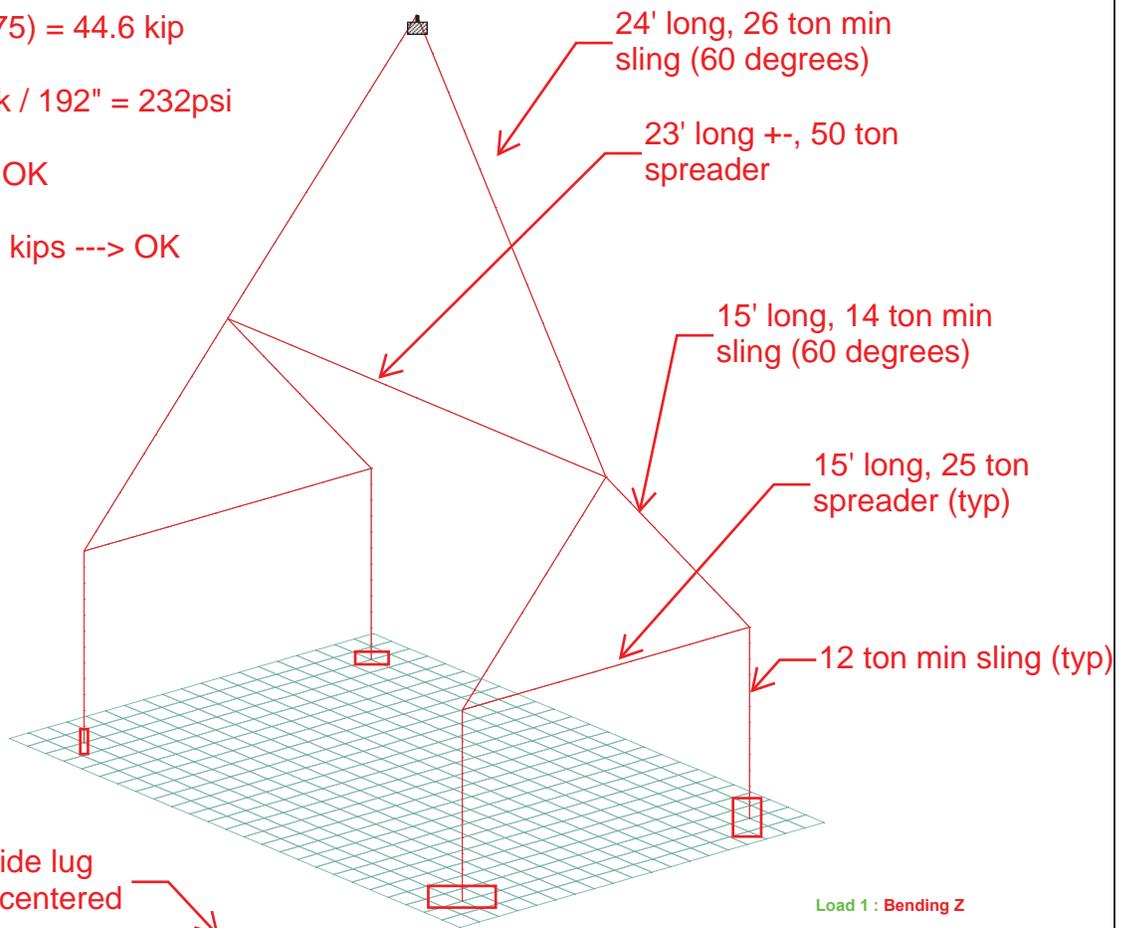
Shear area =  $6" \times 32" = 192"$

$22.3\text{kips} \times 1.5 / (.75) = 44.6 \text{ kip}$

shear load =  $44.6\text{k} / 192" = 232\text{psi}$

$4\sqrt{f'c} = 282 \text{ psi} \rightarrow \text{OK}$

each coil rod = 18 kips  $\rightarrow \text{OK}$

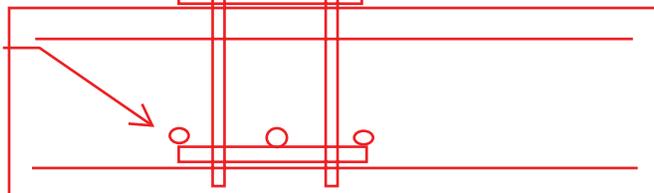


5.5" tall x 6" wide lug with 1.5" hole centered

7/8" coil rod w/nut, 4" o.c.

10" x 6" x 1" grade 50 plate

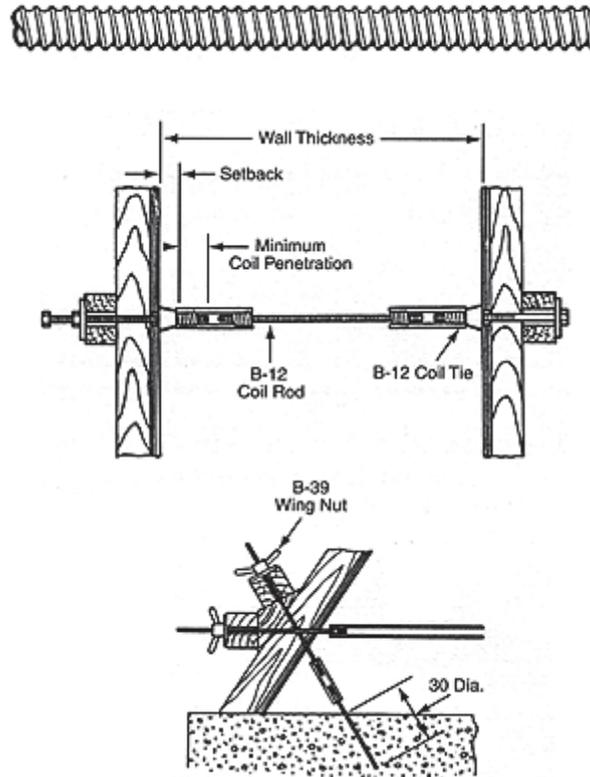
extra #6 bars @ 2' long



## B-12 Coil Rod

Dayton/Richmond B-12 Coil Rod is available in 1/2" to 1-1/2" diameters in 12' lengths. Field cutting can be accomplished with bolt cutters or carborundum blades.

B-12 threaded rod can be used with Coil Ties in many forming combinations to tie formwork, for adjustable ties, for concrete embedments and/or emergency ties.



B-12 Coil Rod Selection Chart						
Coil Rod Diameter	Safe Working Loads		Minimum Root Area (sq. in.)	Tensile Stress (psi.)	Yield Stress (psi.)	Minimum Coil Penetration
	Tension (lbs.)	Shear (lbs.)				
1/2"	9,000	6,000	.1385	130,000	110,000	2"
5/8"	12,000	8,000	.2124	113,000	96,000	2-1/4"
3/4"	18,000	12,000	.3079	117,000	100,000	2-1/4"
7/8"	31,000	20,600	.4477	117,000	100,000	2-1/2"
1"	38,000	25,300	.5410	140,000	120,000	2-1/2"
1-1/8"	45,000	30,000	.7163	126,600	105,000	2-1/2"
1-1/4"	56,000	37,500	.9161	123,000	105,000	2-1/2"
1-1/2"	68,000	45,300	1.3892	98,000	85,000	3"

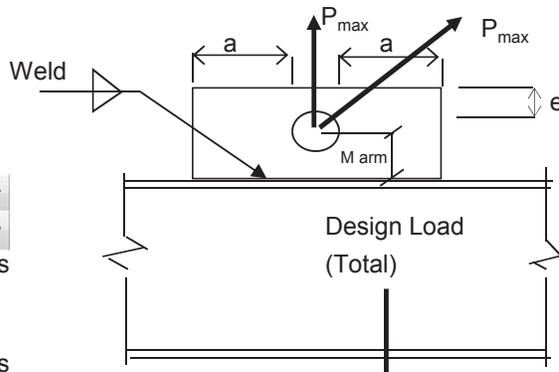
SWL provides a factor of safety of approximately 2 to 1.



CONSTRUCTION LEADERS

**Design of Lifting Beams Connections**

Service Load = **22.3**  
 Impact factor = **1.5**  
**Input:** Design Load = **33.45 Kips**  
 Design Angle = 90  
 # of Legs of Sling = 1  
 d = **1.5 inches**  
 t = **1 inch**  
 $F_u =$  **58 ksi**  
 a = **2 inches**  
 $F_y =$  **36 ksi**  
 e = **2 inches**  
 h = **5.5 inches**  
 l = **6 inches**



px = 0.00 kips  
 py = 33.45 kips  
 Pmax = 33.45 kips

**Ultimate Tensile Load**

$P_u = 2*a*t*F_u = 232.0$  kips  
 $P_{allow} = 0.20*P_u = 46.40$  kips

**Design Load is O.K.!**  
**46.40 > 33.45**

**Lug Tearout ( $P_{max}$  Diagonal)**

Load Factor = 1  
 $P_{allow} = 1.67*F_b*t*e^2/d = 105.81$  kips  
 $e_{min} = 1.01$  inches

**Design Load is O.K.!**  
**105.81 > 33.45**

**Allowable Crushing**

$P_p = 0.9*F_y*t*d = 48.60$  kips

**Design Load is O.K.!**  
**48.60 > 33.45**

**Shear**

$P_u = 2*(0.4)*F_y*e*t = 57.60$  kips

**Design Load is O.K.!**  
**57.60 > 33.45**

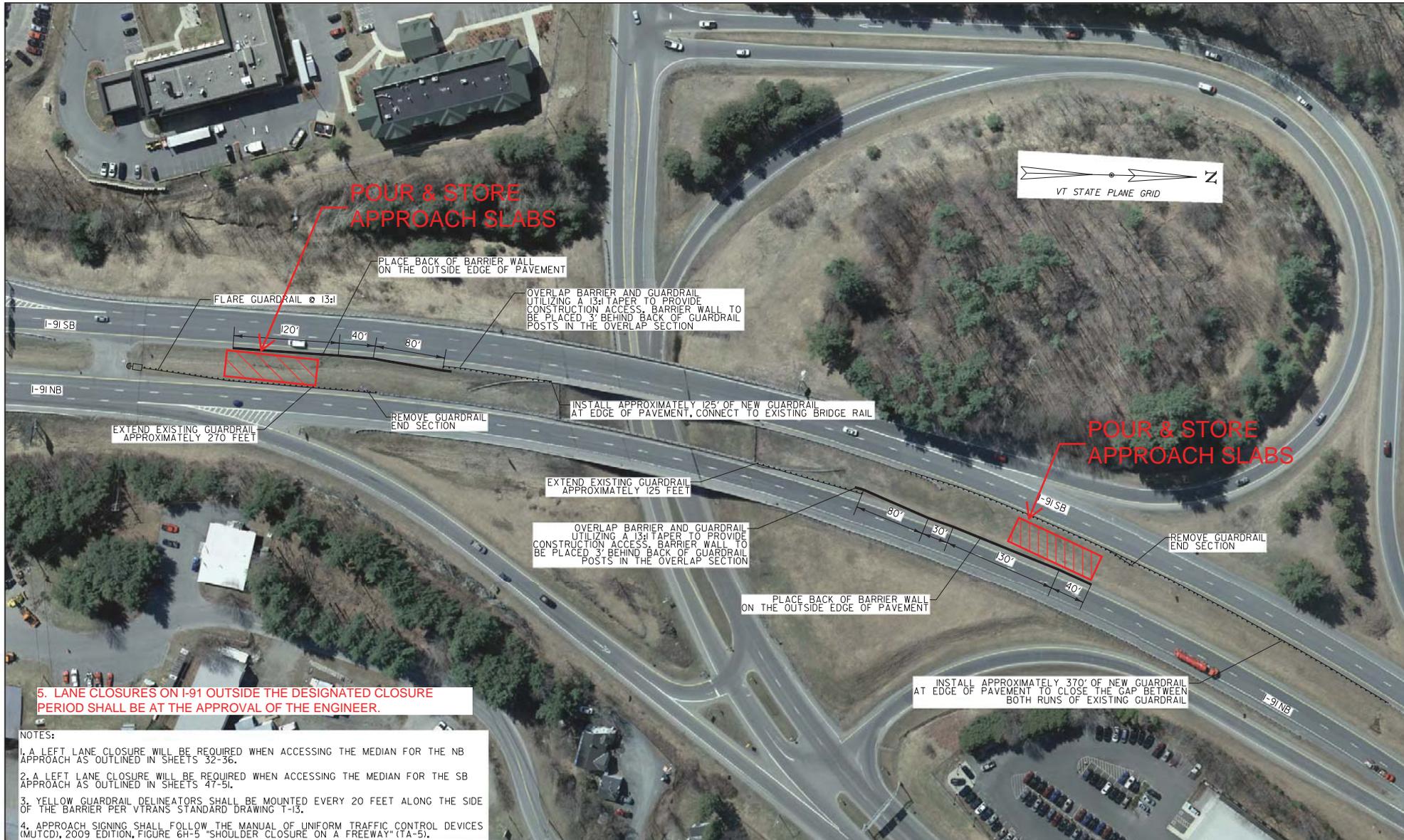
**Weld Design**

$M_{arm} = 2.75$  inches  
 $S_w = d^2/3 = 10.08$  in<sup>2</sup>  
 $A_w = 11$  in

$f_m = 0.00$  kips/inch  
 $f_v = 3.04$  kips/inch  
 $f_t = 0.00$  kips/inch  
 $f_w = 3.04$  kips/inch

**use 1/4 fillet weld**

# **POUR & STORAGE LOCATION**



5. LANE CLOSURES ON I-91 OUTSIDE THE DESIGNATED CLOSURE PERIOD SHALL BE AT THE APPROVAL OF THE ENGINEER.

- NOTES:
1. A LEFT LANE CLOSURE WILL BE REQUIRED WHEN ACCESSING THE MEDIAN FOR THE NB APPROACH AS OUTLINED IN SHEETS 32-36.
  2. A LEFT LANE CLOSURE WILL BE REQUIRED WHEN ACCESSING THE MEDIAN FOR THE SB APPROACH AS OUTLINED IN SHEETS 47-51.
  3. YELLOW GUARDRAIL DELINEATORS SHALL BE MOUNTED EVERY 20 FEET ALONG THE SIDE OF THE BARRIER PER VTRANS STANDARD DRAWING T-13.
  4. APPROACH SIGNING SHALL FOLLOW THE MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES (MUTCD), 2009 EDITION, FIGURE 6H-5 "SHOULDER CLOSURE ON A FREEWAY" (TA-5).



Vermont Agency of Transportation  
**RECEIVED**  
 CK'D BY: CB/NA    CK'D BY: JS  
 April 23, 2015  
 RESUBMIT: NO    Approved As Noted  
 BY: NH    DATE: 4-24-2015

I-91 MEDIAN WORK

SCALE 1" = 50' - 0"  
 50 0 50

PROJECT NAME: HARTFORD  
 PROJECT NUMBER: IM 091-2(79)



PREPARED BY:  
 FILE NAME: si2a026\_Median Closure.dgn  
 PROJECT LEADER: K. HIGGINS  
 DESIGNED BY: B. LYON  
 I-91 MEDIAN WORK  
 PLOT DATE: 04/23/15  
 DRAWN BY: B. LYON  
 CHECKED BY: S. SAWYER  
 SHEET 70 OF 77

# **ERECTION CALCS (CRANE LIFT CHARTS)**



EA

APPROACH SLAB FORMWORK

$D = 15''$

$P_{max} = 1.25' (150 \text{ lbs/ft}^3) = 187.5 \text{ lbs/ft}^2$

PLYWOOD

SPACE SUPPORTS @ 24" O.C. MAX OK - REF SHEET 2

2x4 STUDS

$P_{max} = 187.5 \text{ lbs/ft}^2 \times 2' = 375 \text{ lbs/ft}$

$M_{max} = \frac{WL^2}{8} = \frac{375 \frac{\text{lbs}}{\text{ft}} (1.25')^2}{8} = 73 \text{ lb.ft}$

$V_{max} = \frac{WL}{2} = \frac{375 \text{ lbs/ft} (1.25')}{2} = 234 \text{ lbs}$

$P_{max} = 375 \text{ lbs/ft} \times 1.25' = 469 \text{ lbs (POSTS)}$

OK REF SHEET 3



**CONSTRUCTION LEADERS**

**PLYWOOD CHECK**

DATE 5/2/2015

SHEET 1 OF 1

INITIAL EH

**Plywood Design:**

Number of Spans = 3 or more

Dead Load Pressure = 187.5 lb/ft<sup>2</sup>  
 Live Load Pressure = 0 lb/ft<sup>2</sup>  
 Pressure Applied = 187.5 lb/ft<sup>2</sup>  
 Joist Spacing = 24 in.  
 Support Width = 1.5 in.  
 $I_s = 22.5$  in.  
 $I_d = 22.75$  in.  
 $L = 270$  0.089 in.

Sheathing Section Properties:

Type: Plyform

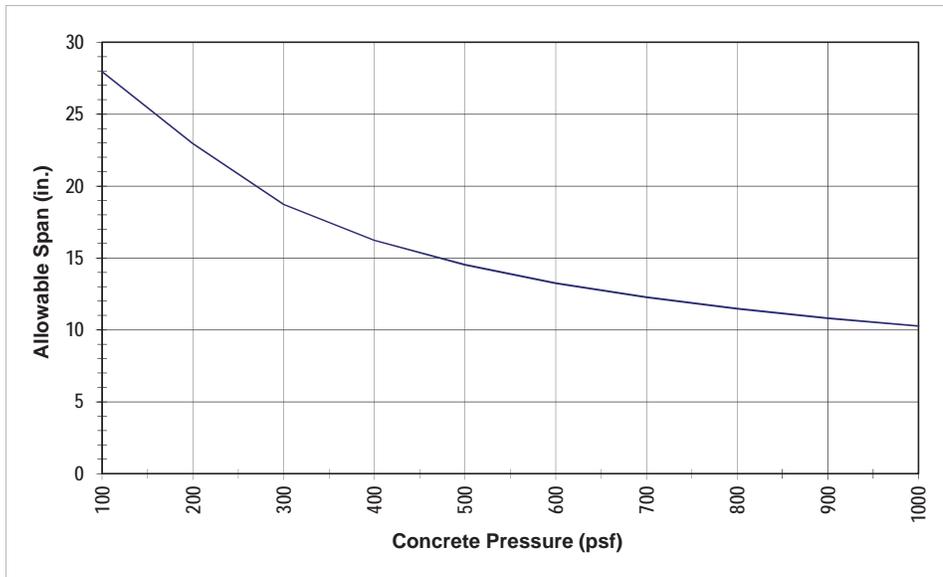
Thickness 3/4

Face Grain Direction: Across Supports

$t = 0.75$  in.  
 $I = 0.199$  in<sup>4</sup>/ft.  
 $KS = 0.455$  in<sup>3</sup>/ft.  
 $lb/Q = 7.187$  in<sup>2</sup>/ft.  
 $F_b = 1,930$  lb/in<sup>2</sup>  
 $F_v = 72$  lb/in<sup>2</sup>  
 $E = 1,650,000$  lb/in<sup>2</sup>  
 $E_c = 1,500,000$  lb/in<sup>2</sup>  
 $C = 120$

Design Pressure $p$ (lb/ft <sup>2</sup> )	Maximum Center to Center Spacing of Supports				Limiting Span $L$ (in.)
	Based on Bending Stress	Based on Bending Deflection	Based on Rolling Shear	Based on Shear Deflection	
	$L$ (in.)	$L$ (in.)	$L$ (in.)	$L$ (in.)	
100	32.46	27.96	104.99	209.51	27.96
200	22.95	23.71	53.25	105.50	22.95
300	18.74	21.54	36.00	70.84	18.74
400	16.23	20.13	27.37	53.50	16.23
500	14.52	19.11	22.20	43.10	14.52
600	13.25	18.31	18.75	36.17	13.25
700	12.27	17.67	16.28	31.22	12.27
800	11.48	17.13	14.44	27.50	11.48
900	10.82	16.67	13.00	24.61	10.82
1000	10.27	16.27	11.85	22.30	10.27
187.5	23.71	24.07	56.70	112.44	23.71

Use 24" (MAX)  
 MAX PRESSURE ONLY AT  
 VERY BOTTOM



# 2X4 CHECK

## TIMBER BEAM-COLUMN DESIGN ASD NDS 2001

ENGINEER: EWH      DATE 5/2/15

CHK BY:      DATE

LOADS	DESIGN PARAMETERS		MEMBER DIMENSIONS	
R = 234 Lb	Le = 1.25 ft	Lx = 1.25 ft	bx = 1.5 in	
V = 234 Lb	Lb = 3.5 in	Kx = 1.0	dy = 3.5 in	
Mx = 73 Ft - Lb	BRG LOCATION = END	Ly = 1.25 ft	NOTCH = 0 in	
My = Ft - Lb	BRG FACE = WIDTH bx	Ky = 1.0	FULLY BRACED = No	
P = 469 Lb		BRACED WEAK AXIS = No	CANTILEVER = No	
Δ = 0.00 in.				

### PROPERTIES

Species : **Southern Pine**

		ADJUSTMENT FACTORS NDS 4.3			
F <sub>b</sub> = 1500 psi	C <sub>D</sub> = 1.25	C <sub>i</sub> = 1.00	Area = 5.25 in <sup>2</sup>	K <sub>be</sub> = 0.439	
F <sub>V</sub> = 175 psi	C <sub>M</sub> = 1.00	C <sub>r</sub> = 1.15	I <sub>x</sub> = 5.359 in <sup>4</sup>	KcE = 0.3	
F <sub>c</sub> = 1650 psi	C <sub>t</sub> = 1.00	C <sub>f</sub> = 1.00	I <sub>y</sub> = 0.984 in <sup>4</sup>	c = 0.8	
F <sub>c</sub> perp = 565 psi	C <sub>F</sub> = 1.00	C <sub>T</sub> = 1.00	S <sub>x</sub> = 3.063 in <sup>3</sup>		
E = 1500000 psi	C <sub>fu</sub> = 1.00		S <sub>y</sub> = 1.313 in <sup>3</sup>		
			E' = 1500000 psi		

### BEAM AND COLUMN DESIGN

#### STRONG AXIS BENDING NDS SEC. 3.3

$$F_b' = F_b \cdot C_D \cdot C_M \cdot C_t \cdot C_F \cdot C_L \cdot C_i \cdot C_r \cdot C_t \quad (\text{TABLE 4.3.1})$$

$$Lb/dy = 4.28571$$

$$\text{APPROX. } le = 30.9 \text{ in (for uniform loads) (TABLE 3.3.3)}$$

$$R_B = 6.93301 \text{ (NDS eq. 3.3-5)}$$

$$F_b^* = 2156.25 \text{ psi}$$

$$F_{bE} = 13699.7 \text{ psi}$$

$$C_L = 0.85 \text{ (NDS eq. 3.3-6)}$$

$f_{bx} = 286.04 \text{ psi}$
$F'_{bx} = 1840.74 \text{ psi}$

**CHECK**  
**OK**      % OF CAPACITY  
15.54%

#### WEAK AXIS (FLAT USE) BENDING NDS SEC. 3.3

$$F_b' = F_b \cdot C_D \cdot C_M \cdot C_t \cdot C_F \cdot C_L \cdot C_{fu} \cdot C_i \cdot C_r \cdot C_t \quad (\text{TABLE 4.3.1})$$

$f_{by} = 0.00 \text{ psi}$
$F'_{by} = 2156.25 \text{ psi}$

**CHECK**  
**OK**      % OF CAPACITY  
0.00%

#### SHEAR NDS SEC. 3.4

$$F_v' = F_v \cdot C_D \cdot C_M \cdot C_t \cdot C_i \quad (\text{TABLE 4.3.1})$$

$$\text{NDS 3.2.3.2 - Allowable notch} = 1/4 \cdot d = 0.88$$

$$d_n^* = 3.5 \text{ in}$$

$f_v = 66.86 \text{ psi}$
$F_v' = 218.75 \text{ psi}$

**CHECK**  
**OK**      % OF CAPACITY  
30.56%

$$\text{ALLOWABLE V FOR NOTCH TENSION FACE 3.4.3.2} = 766 \text{ Lb. (NDS eq. 3.4-3)}$$

#### COMPRESSION NDS SEC. 3.7

$$F_c' = F_c \cdot C_D \cdot C_M \cdot C_t \cdot C_F \cdot C_i \cdot C_P \quad (\text{TABLE 4.3.1})$$

$$le_1 = 15 \text{ in} \quad le_1/d_1 = 4.29 \quad \text{O.K.! NDS SEC. 3.7.1.4}$$

$$le_2 = 15.00 \text{ in} \quad le_2/d_2 = 10.00 \quad \text{O.K.! NDS SEC. 3.7.1.4}$$

$$F_c^* = 2062.50 \text{ psi}$$

$$C_{P1} = 0.98$$

$$F_{cE1} = KcE'E/(le_1/d_1)^2 = 24500.00 \text{ psi}$$

$$C_{P2} = 0.88 \quad \text{CONTROLS}$$

$$F_{cE2} = KcE'E/(le_2/d_2)^2 = 4500.00 \text{ psi}$$

$fc = 89.33 \text{ psi}$
$F_c' = 1816.56 \text{ psi}$

**CHECK**  
**OK**      % OF CAPACITY  
4.92%

$$F_{cE1} / F_c^* = 11.88$$

$$F_{cE2} / F_c^* = 2.18$$

#### COMPRESSION PERPENDICULAR TO GRAIN NDS SEC. 3.7

$$F_c' \text{ (perp)} = F_c \text{ (perp)} \cdot C_M \cdot C_t \cdot C_i \cdot C_b \quad (\text{TABLE 4.3.1})$$

$$\text{Area} = 5.25 \text{ in}^2$$

$$x = 1.5 \text{ in}$$

$$Lb = 3.5 \text{ in}$$

$$Cb = 1.11 \quad \text{NDS SEC. 3.10.4}$$

$fc \text{ (perp)} = 44.57 \text{ psi}$
$F_c' \text{ (perp)} = 565.00 \text{ psi}$

**CHECK**  
**OK**      % OF CAPACITY  
7.89%

#### INTERACTION EQUATION NDS SEC 3.9

$$f_c < F_{cE1} = \text{OK FOR EITHER UNAXIAL OR BIAXIAL BENDING}$$

$$f_c < F_{cE2} = \text{OK FOR EITHER UNAXIAL OR BIAXIAL BENDING}$$

$$f_{b1} < F_{bE} = \text{OK FOR BIAXIAL BENDING}$$

$$\left[ \frac{f_c}{F_c'} \right]^2 + \frac{f_{b1}}{F_{b1} \left[ 1 - \left( \frac{f_c}{F_{cE1}} \right) \right]} + \frac{f_{b2}}{F_{b2} \left[ 1 - \left( \frac{f_c}{F_{cE2}} \right) - \left( \frac{f_{b1}}{F_{bE}} \right)^2 \right]} = 0.16 \quad \text{OK} \quad \img alt="green checkmark" style="vertical-align: middle;"/>$$

#### DEFLECTION

$$\Delta = \text{L/ \#DIV/0!}$$

L/120 = 0.13	O.K.!
L/270 = 0.06	O.K.!
L/360 = 0.04	O.K.!

## CRANE LIFT STUDY ANALYSIS - LONG FORM (page 1)

**Project:** Hartford Lateral Slide

**Name:** Erich Heymann

**Date/Time:** 5/16/2015

### Load Information

What is to be lifted? Approach Slabs is more than one crane required? No

Initial Location: Attach Lift Diagram (Plan View)

Final Set Location: Attach Lift Diagram (Plan View)

Verified Weight (Weight of Load) 85,928 How was weight verified? Calculation

Lift Points

Per Manufacturer

Other, attach details and calculations

Maximum radius of lift 48' Quadrants 4

Maximum Elevation of Lift: Attach Lift Diagram, (Elevation View)

Maximum Allowable Wind Speed for Lift. 35 Mph

**Ground Conditions:** Nature of Soil Crane Mats Safe Bearing Capacity 1 (tpsf)

Is the use of crane mats, or compacted fill required? Yes X No       

### Crane Configuration

Model/Serial # Link-Belt 298 HSL Boom Length/Type 140'

Maximum Capacity 250 Ton Jib Length/Type N/A

Boom Point Elevation at Maximum Working Radius 141'

Cable Diameter 1" Block Capacity 165 Ton Number of Parts 8

Anti-two block device: Yes X No        Crane/Barge List 0

### Calculations

Weight of Load 85,928 + Rigging Weight 3,580 + Crane Capacity Deductions 6,797

= Gross Weight 96,305

Maximum Lift Capacity for Radius = 124,200

% of Crane Chart 78% (Gross weight/Crane Capacity) SEE **DISTRICT POLICY**

### Responsible Personnel (Print Name & Sign)

Project Manager: \_\_\_\_\_

Level 1 Lift Specialist: \_\_\_\_\_

Level 2 Lift Specialist: \_\_\_\_\_

Level 3 Lift Specialist: (IF Req'd) \_\_\_\_\_

Superintendent: \_\_\_\_\_

Operator: \_\_\_\_\_



**CRANE LIFT STUDY ANALYSIS - LONG FORM (page 2)**

**WORKSHEET**

**Rigging**

Sling Length \_\_\_\_\_ Vertical Length \_\_\_\_\_ Sling Angle \_\_\_\_\_ Sling Load Angle Factor \_\_\_\_\_

	<u>Type/Length</u>	<u>Size</u>	<u>Capacity</u>	<u>Quantity</u>	<u>Weight</u>
50 Ton Spreader	N/A	N/A	50 Ton	1	1,400
25 Ton Spreaders	N/A	N/A	25 Ton	2	1,000
28 Ton Slings	20'	1-3/4"	26 Ton	2	250
15 Ton Slings	16'	1-1/4"	14 Ton	4	200
12 Ton Slings	10'	1-1/8"	12 Ton	4	100
35 Ton Shackles	Anchor Shackle	2"	35 Ton	4	180
17 Ton Shackles	Anchor Shackle	1-1/2"	17 Ton	4	70
12 Ton Shackles	Anchor Shackle	1-1/4"	12 Ton	8	80
Lifting Lugs	Complete Setup	N/A	N/A	4	300

**TOTAL WEIGHT OF RIGGING** \_\_\_\_\_ 3,580

**Crane Capacity Deductions**

Gross Weight of:

Block	<u>3,392</u>
Effective Jib Weight	<u>0</u>
Upper Boom Pt.	<u>0</u>
Hook and Overhaul Ball	<u>1,255</u>
Whip Line Below Boom Tip	<u>50</u>
Main Load Cable Below Tip (8 Part)	<u>2,100</u>
Stowed Jib or Boom Extension	<u>0</u>
<b>TOTAL DEDUCTIONS:</b>	<u>6,797</u>

**Final Checks Prior to Start**

- Verify Gross Weight and Load Chart Capacities, (De-rated if Crane on Barge)
- Inspected Crane and Verified Components (Daily Logs and Annual Certification Checked)
- Inspected Rigging for Condition and Size
- Ground Stability. Outrigger pads/blocking sized correctly? Barge/Crane List, (Derated Chart?)
- Distance to Nearest Utility (above and below ground)
- Weather and wind load considerations, checked and verified at time of lift.
- Pre-Lift Meeting and Rigging Crew, Operator, and Signal Person (Attach sign-in sheet)
- Rigging Drawings Attached
- Method of Communication, (radios, hand signals etc.) checked & verified
- Lift Abort Procedures, checked and verified. JHA/PSI conducted

## CRANE LIFT STUDY ANALYSIS - LONG FORM (page 1)

**Project:** Hartford Lateral Slide

**Name:** Erich Heymann

**Date/Time:** 5/16/2015

### Load Information

What is to be lifted? Approach Slabs is more than one crane required? No

Initial Location: Attach Lift Diagram (Plan View)

Final Set Location: Attach Lift Diagram (Plan View)

Verified Weight (Weight of Load) 85,928 How was weight verified? Calculation

Lift Points

Per Manufacturer

Other, attach details and calculations

Maximum radius of lift 35' Quadrants 4

Maximum Elevation of Lift: Attach Lift Diagram, (Elevation View)

Maximum Allowable Wind Speed for Lift. 35 Mph

**Ground Conditions:** Nature of Soil Crane Mats Safe Bearing Capacity 1 (tpsf)

Is the use of crane mats, or compacted fill required? Yes X No       

### Crane Configuration

Model/Serial # Link-Belt LS-248H II Boom Length/Type 120'

Maximum Capacity 200 Ton Jib Length/Type N/A

Boom Point Elevation at Maximum Working Radius 123'

Cable Diameter 7/8" Block Capacity 60 Ton Number of Parts 4

Anti-two block device: Yes X No        Crane/Barge List 0

### Calculations

Weight of Load 85,928 + Rigging Weight 3,580 + Crane Capacity Deductions 3,615

= Gross Weight 93,123

Maximum Lift Capacity for Radius = 128,900

% of Crane Chart 72% (Gross weight/Crane Capacity) SEE **DISTRICT POLICY**

### Responsible Personnel (Print Name & Sign)

Project Manager: \_\_\_\_\_

Level 1 Lift Specialist: \_\_\_\_\_

Level 2 Lift Specialist: \_\_\_\_\_

Level 3 Lift Specialist: (IF Req'd) \_\_\_\_\_

Superintendent: \_\_\_\_\_

Operator: \_\_\_\_\_



**CRANE LIFT STUDY ANALYSIS - LONG FORM (page 2)**

**WORKSHEET**

**Rigging**

Sling Length \_\_\_\_\_ Vertical Length \_\_\_\_\_ Sling Angle \_\_\_\_\_ Sling Load Angle Factor \_\_\_\_\_

	<u>Type/Length</u>	<u>Size</u>	<u>Capacity</u>	<u>Quantity</u>	<u>Weight</u>
50 Ton Spreader	N/A	N/A	50 Ton	1	1,400
25 Ton Spreaders	N/A	N/A	25 Ton	2	1,000
28 Ton Slings	20'	1-3/4"	26 Ton	2	250
15 Ton Slings	16'	1-1/4"	14 Ton	4	200
12 Ton Slings	10'	1-1/8"	12 Ton	4	100
35 Ton Shackles	Anchor Shackle	2"	35 Ton	4	180
17 Ton Shackles	Anchor Shackle	1-1/2"	17 Ton	4	70
12 Ton Shackles	Anchor Shackle	1-1/4"	12 Ton	8	80
Lifting Lugs	Complete Setup	N/A	N/A	4	300

**TOTAL WEIGHT OF RIGGING** \_\_\_\_\_ 3,580

**Crane Capacity Deductions**

Gross Weight of:

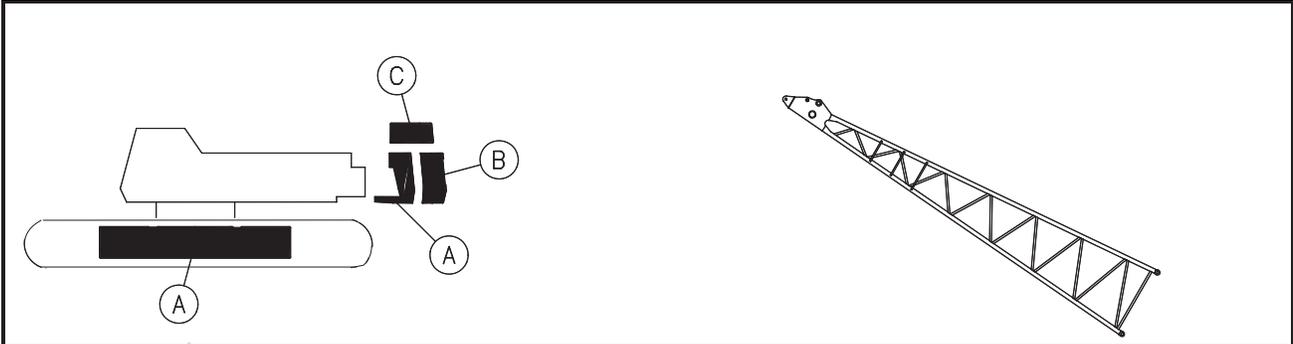
Block	<u>1,650</u>
Effective Jib Weight	<u>0</u>
Upper Boom Pt.	<u>0</u>
Hook and Overhaul Ball	<u>1,215</u>
Whip Line Below Boom Tip	<u>50</u>
Main Load Cable Below Tip (4 Part)	<u>700</u>
Stowed Jib or Boom Extension	<u>0</u>
<b>TOTAL DEDUCTIONS:</b>	<u>3,615</u>

**Final Checks Prior to Start**

- Verify Gross Weight and Load Chart Capacities, (De-rated if Crane on Barge)
- Inspected Crane and Verified Components (Daily Logs and Annual Certification Checked)
- Inspected Rigging for Condition and Size
- Ground Stability. Outrigger pads/blocking sized correctly? Barge/Crane List, (Derated Chart?)
- Distance to Nearest Utility (above and below ground)
- Weather and wind load considerations, checked and verified at time of lift.
- Pre-Lift Meeting and Rigging Crew, Operator, and Signal Person (Attach sign-in sheet)
- Rigging Drawings Attached
- Method of Communication, (radios, hand signals etc.) checked & verified
- Lift Abort Procedures, checked and verified. JHA/PSI conducted

# 298 HSL

<b>Main Boom Capacities - 140 Ft Open Throat Tube Boom</b>							
Load Radius (ft)	Boom Angle (deg)	Over End Blocked	360 Degree Rotation				Load Radius (ft)
		ABCDE+A	ABCDE+A	ABCD+A	ABC+A	AB+A	
		CURVE 1	CURVE 2	CURVE 3	CURVE 4	CURVE 5	
23.94	82.0	277,800	277,800	277,800	269,700	243,000	23.94
25	81.6	274,300	274,300	269,600	257,500	225,500	25
30	79.5	228,800	228,800	215,600	191,500	167,400	30
35	77.4	190,300	190,300	171,000	151,700	132,400	35
40	75.3	160,800	157,300	141,200	125,100	109,000	40
<b>41</b>	<b>74.9</b>	<b>157,000</b>	<b>153,100</b>	<b>137,400</b>	<b>121,700</b>	<b>106,000</b>	<b>41</b>
<b>42</b>	<b>74.4</b>	<b>153,300</b>	<b>149,000</b>	<b>133,700</b>	<b>118,400</b>	<b>103,100</b>	<b>42</b>
<b>43</b>	<b>74.0</b>	<b>149,600</b>	<b>144,900</b>	<b>130,000</b>	<b>115,100</b>	<b>100,200</b>	<b>43</b>
<b>44</b>	<b>73.6</b>	<b>145,900</b>	<b>140,700</b>	<b>126,200</b>	<b>111,700</b>	<b>97,200</b>	<b>44</b>
<b>45</b>	<b>73.2</b>	<b>142,200</b>	<b>136,600</b>	<b>122,500</b>	<b>108,400</b>	<b>94,300</b>	<b>45</b>
<b>46</b>	<b>72.7</b>	<b>138,400</b>	<b>132,500</b>	<b>118,800</b>	<b>105,100</b>	<b>91,400</b>	<b>46</b>
<b>47</b>	<b>72.3</b>	<b>134,700</b>	<b>128,300</b>	<b>115,000</b>	<b>101,700</b>	<b>88,400</b>	<b>47</b>
<b>48</b>	<b>71.9</b>	<b>131,000</b>	<b>124,200</b>	<b>111,300</b>	<b>98,400</b>	<b>85,500</b>	<b>48</b>
<b>49</b>	<b>71.4</b>	<b>127,300</b>	<b>120,100</b>	<b>107,600</b>	<b>95,100</b>	<b>82,600</b>	<b>49</b>
50	71.0	123,600	116,000	103,900	91,800	79,700	50
<b>51</b>	<b>70.6</b>	<b>121,000</b>	<b>113,500</b>	<b>101,600</b>	<b>89,700</b>	<b>77,900</b>	<b>51</b>
<b>52</b>	<b>70.1</b>	<b>118,500</b>	<b>111,000</b>	<b>99,400</b>	<b>87,700</b>	<b>76,100</b>	<b>52</b>
<b>53</b>	<b>69.7</b>	<b>116,000</b>	<b>108,500</b>	<b>97,100</b>	<b>85,700</b>	<b>74,300</b>	<b>53</b>
<b>54</b>	<b>69.2</b>	<b>113,500</b>	<b>106,000</b>	<b>94,900</b>	<b>83,700</b>	<b>72,600</b>	<b>54</b>
<b>55</b>	<b>68.8</b>	<b>111,000</b>	<b>103,500</b>	<b>92,600</b>	<b>81,700</b>	<b>70,800</b>	<b>55</b>
<b>56</b>	<b>68.4</b>	<b>108,500</b>	<b>101,000</b>	<b>90,400</b>	<b>79,700</b>	<b>69,000</b>	<b>56</b>
<b>57</b>	<b>67.9</b>	<b>106,000</b>	<b>98,500</b>	<b>88,100</b>	<b>77,700</b>	<b>67,300</b>	<b>57</b>
<b>58</b>	<b>67.5</b>	<b>103,500</b>	<b>96,000</b>	<b>85,900</b>	<b>75,700</b>	<b>65,500</b>	<b>58</b>
<b>59</b>	<b>67.0</b>	<b>101,000</b>	<b>93,500</b>	<b>83,600</b>	<b>73,700</b>	<b>63,700</b>	<b>59</b>
60	66.6	98,500	91,100	81,400	71,700	62,000	60
70	62.1	82,700	74,400	66,400	58,300	50,200	70
80	57.3	69,700	62,500	55,600	48,700	41,800	80
90	52.3	59,800	53,600	47,500	41,500	35,400	90
100	47.0	52,000	46,600	41,200	35,800	30,400	100
110	41.1	46,900	41,000	36,200	31,300	26,400	110
120	34.4	41,100	36,400	32,000	27,600	23,200	120
130	26.3	36,200	32,500	28,500	24,400	20,400	130
136.02	20.0	33,400	30,500	26,600	22,800	18,900	136.02



**MAIN BOOM CAPACITIES - 120 FT OPEN THROAT TUBE BOOM**

Load Radius (ft)	Boom Angle (deg)	360° Rotation					Over End Blocked	Load Radius (ft)
		ABC + A CTWT (lb)	ABC CTWT (lb)	AB CTWT (lb)	A CTWT (lb)	0 CTWT (lb)	ABC + A CTWT (lb)	
20.0	82.0	186,200	186,200	186,200	148,900	106,900	186,200	20.0
25	79.6	173,900	173,900	157,300	97,900	69,800	173,900	25
30	77.1	156,900	144,900	117,000	72,200	51,000	156,900	30
35	74.7	128,900	115,000	92,600	56,700	39,700	131,100	35
40	72.2	106,500	94,900	76,300	46,300	32,100	112,600	40
50	67.1	78,500	69,800	55,800	33,200	22,600	86,900	50
60	61.8	61,600	54,600	43,400	25,400	16,800	69,300	60
70	56.2	50,300	44,500	35,100	20,100	13,000	58,300	70
80	50.3	42,200	37,200	29,200	16,300	10,200	49,000	80
90	43.7	36,100	31,800	24,700	13,400	8,100	41,800	90
100	36.3	31,400	27,500	21,200	11,200	6,400	36,100	100
110	27.2	27,500	24,000	18,400	9,400	5,100	31,400	110
120	13.4	24,300	21,100	16,000	7,800	3,900	27,500	120

**Note: Refer To Page 13 For "Capacity Deductions" Caused By Any Jib Attachment Or Tip Extension.**

# **ERECTION DRAWINGS**



### APPROACH SLABS

**GENERAL NOTES**

DRAWINGS SHALL NOT BE SCALED  
 ANY CHANGES TO THE PLAN SHALL BE APPROVED BY THE DESIGN ENGINEER & PROJECT MANAGEMENT  
 CONCRETE MUST ACHIEVE A STRENGTH OF 4250 PSI (85% OF DESIGN STRENGTH) PRIOR TO REMOVAL OF FORMS.  
 CONCRETE MUST ACHIEVE 28 DAY DESIGN STRENGTH (5000 PSI) PRIOR TO BEING MOVED.

**DESIGN AIDS**

-ASD NINTH ED. (STEEL)  
 -AASHTO GUIDE DESIGN SPECIFICATIONS FOR BRIDGE TEMPORARY WORKS

**MATERIAL PROPERTIES**

- CONCRETE
- HPC CLASS A (5 KSI)
- REINFORCING STEEL
- ALL APPROACH SLAB REINFORCING STEEL SHALL BE LEVEL II OR HIGHER.
- HPC RAPID SET
- TBD

**FINISH**

TOP SURFACE OF APPROACH SLABS TO RECEIVE A "TINED" FINISH.

**CURING**

CURING WILL TAKE PLACE IMMEDIATELY UPON COMPLETION OF FINISHING OF THE TOP SURFACE.

THE APPROACH SLABS WILL BE WETTED AND COVERED WITH VISQUEEN/BURLAP FOR A MINIMUM OF 7 DAYS.

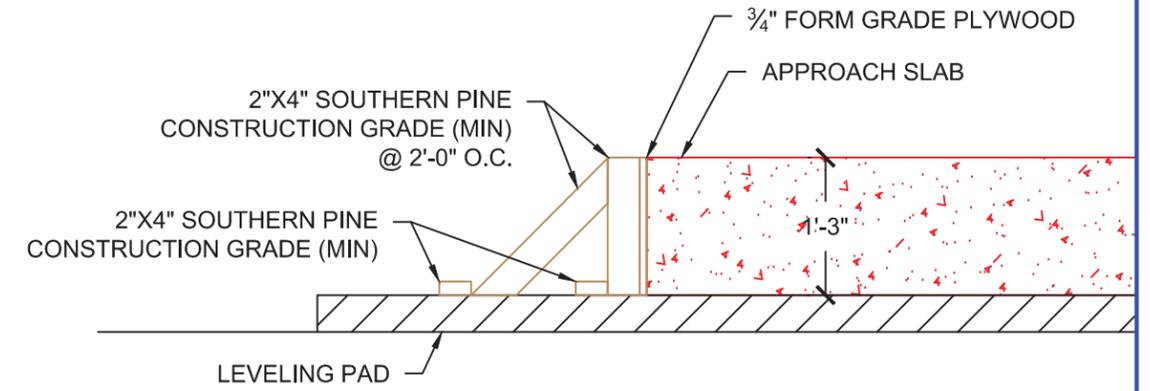
**LIST OF DRAWINGS**

1. TITLE
2. ERECTION PLANS (ABUT 1 & 3)
3. ERECTION PLANS (ABUT 2 & 4)
4. LEVELING PAD & FORMWORK
5. ABUTMENTS 1 & 2 DETAILS
6. ABUTMENTS 3 & 4 DETAILS
7. PT DUCT DETAILS
8. RIGGING DETAILS
9. LIFTING LUG DETAILS

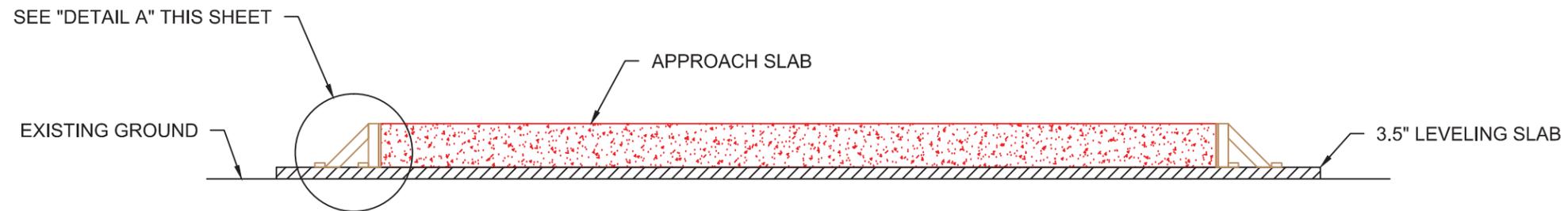
Revision No. & Date	<b>Vermont Agency of Transportation</b>				Drawing Status	Name	Date	<b>PCL Civil Constructors, Inc.</b>	
1 5/26/15					May 27 2015 8:30 PM			3810 Northdale Blvd. Suite 200, Tampa Florida 33624 (813)-264-9500 ; Fax: (813)-264-6689	
	Road No.	County / City	Financial Project ID No.	<b>FOR CONSTRUCTION</b>		Drawn By	Date	Design By	Date
	I-91	Hartford	IM 091-2(79)			EWH	04/13/2015	EWH	04/13/2015
						Check By	Date	TMD	05/05/2015
								Submittal <b>APPROACH SLABS</b>	PCL Project / Job No. I-91 Hartford / 5514001
								Drawing Title <b>TITLE PAGE</b>	Sheet No. 1







**DETAIL A**



**APPROACH SLAB LEVELING PAD & FORMWORK**

Vermont Agency of Transportation

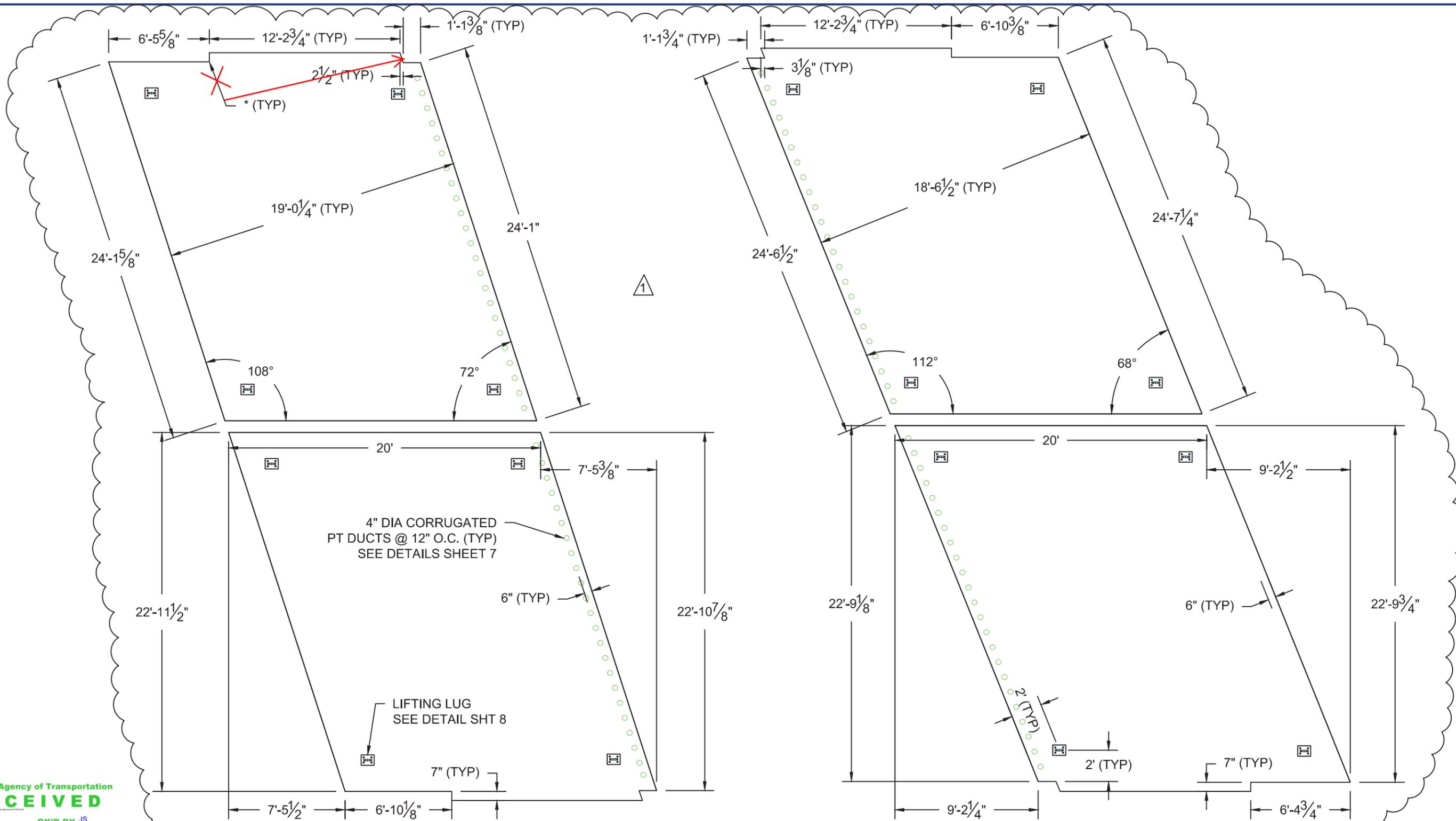
**RECEIVED**

CK'D BY WL OK'D BY JS

May 28, 2015

RESUBMIT NO Approved  
BY KH DATE 6-2-2015

Revision No. & Date	Vermont Agency of Transportation				Drawing Status	Name	Date	PCL Civil Constructors, Inc.	
	Road No.	County / City	Financial Project ID No.		May 27 2015 7:22 PM	Drawn By	EWH	04/13/2015	3810 Northdale Blvd. Suite 200, Tampa Florida 33624 (813)-264-9500 ; Fax: (813)-264-6689
	I-91	Hartford	IM 091-2(79)	<b>FOR CONSTRUCTION</b>	Design By	EWH	04/13/2015	Submittal	PCL Project / Job No.
					Check By	TMD	05/05/2015	APPROACH SLABS	I-91 Hartford / 5514001
								Drawing Title	Sheet No.
								LEVELING PAD & FORMWORK	4



**ABUTMENT 1 APPROACH SLABS**

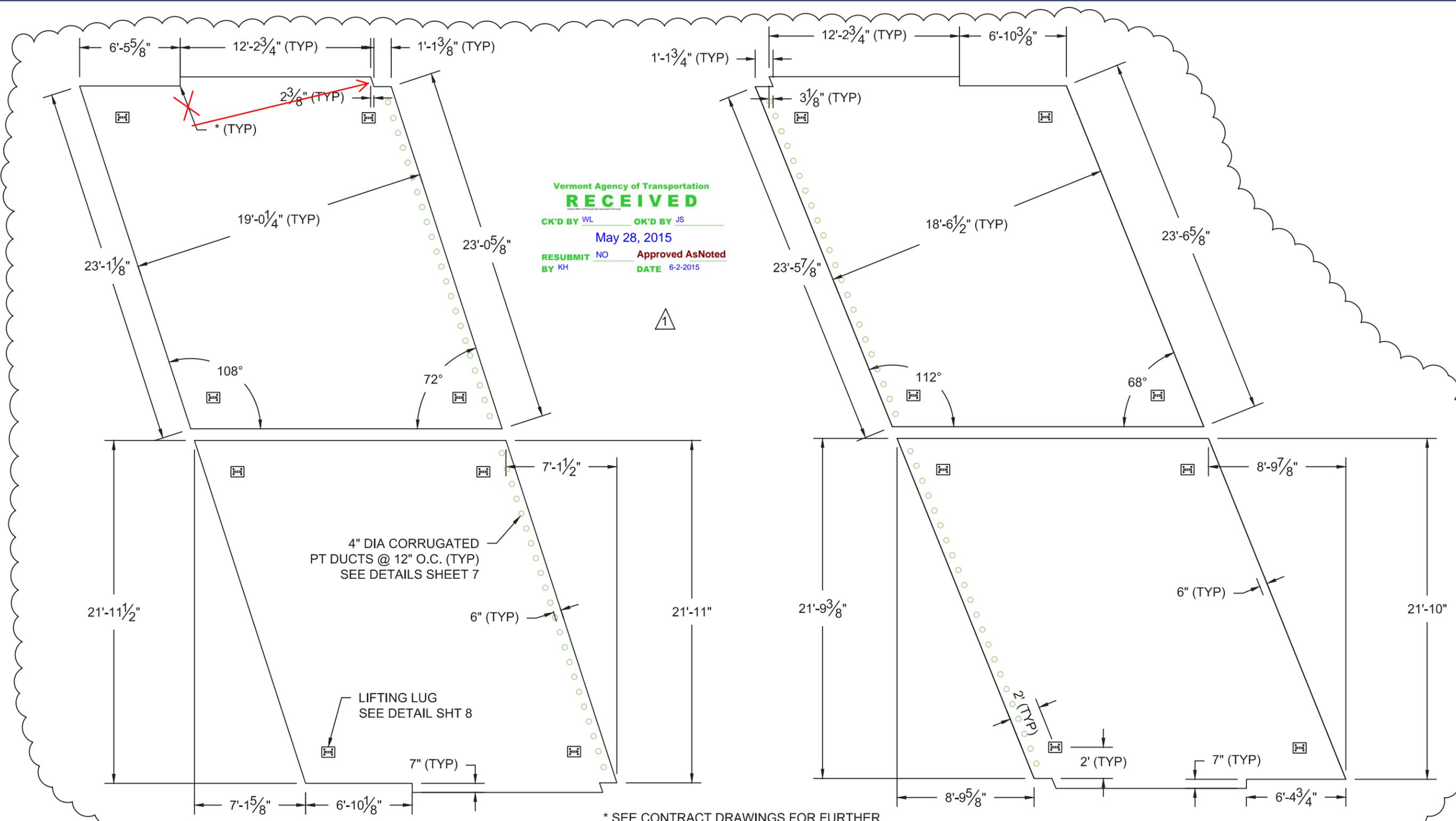
**ABUTMENT 2 APPROACH SLABS**

\* SEE CONTRACT DRAWINGS FOR FURTHER  
DETAIL ON CURB AT BRIDGE RAIL INTERFACE

Vermont Agency of Transportation  
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Revision No. & Date	Vermont Agency of Transportation			Drawing Status	Name	Date	PCL Civil Constructors, Inc.	
1 5/26/15				May 27 2015 7:22 PM	Drawn By	EWH	04/13/2015	3810 Northdale Blvd. Suite 200, Tampa Florida 33624 (813)-264-9500 ; Fax: (813)-264-6689
	Road No.	County / City	Financial Project ID No.	<b>FOR CONSTRUCTION</b>	Design By	EWH	04/13/2015	PCL Project / Job No. I-91 Hartford / 5514001
	I-91	Hartford	IM 091-2(79)		Check By	TMD	05/05/2015	Sheet No. 5
								Drawing Title APPROACH SLABS 1 & 2



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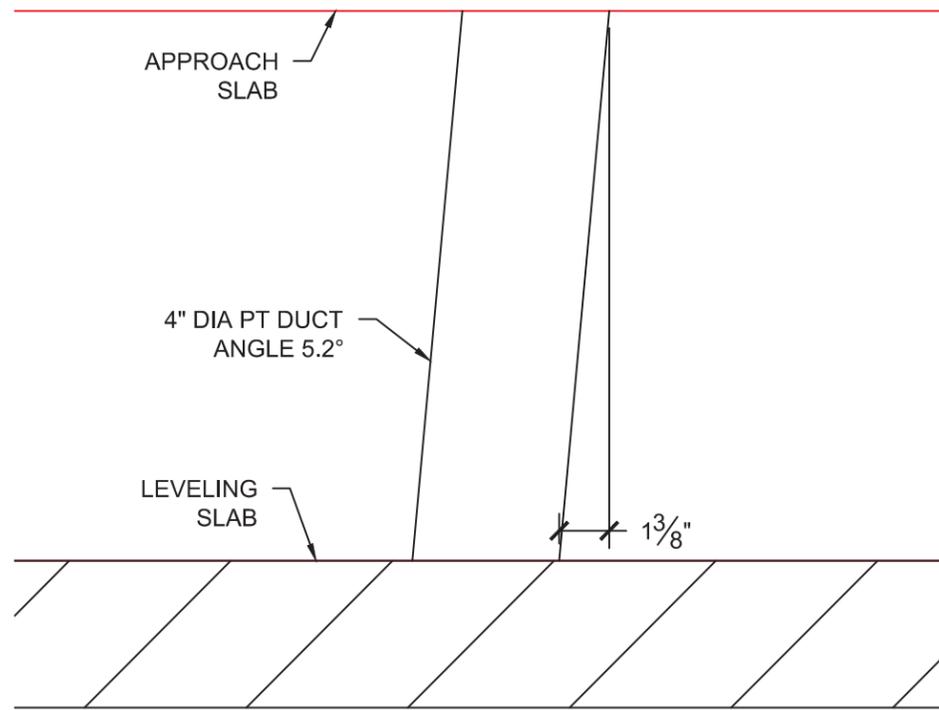
1

**ABUTMENT 3 APPROACH SLABS**

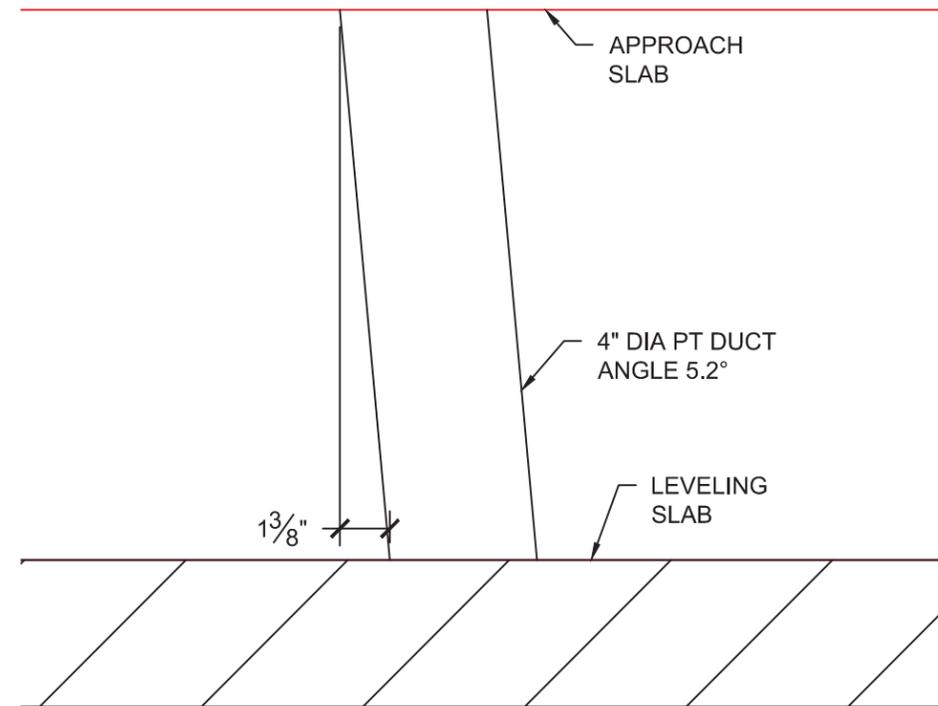
**ABUTMENT 4 APPROACH SLABS**

\* SEE CONTRACT DRAWINGS FOR FURTHER  
 DETAIL ON CURB AT BRIDGE RAIL INTERFACE

Revision No. & Date	Vermont Agency of Transportation				Drawing Status	Name	Date	PCL Civil Constructors, Inc.	
1 5/26/15	Road No.	County / City	Financial Project ID No.		May 27 2015 7:22 PM	Drawn By	EWH	04/13/2015	3810 Northdale Blvd. Suite 200, Tampa Florida 33624 (813)-264-9500 ; Fax: (813)-264-6689
	I-91	Hartford	IM 091-2(79)	<b>FOR CONSTRUCTION</b>	Design By	EWH	04/13/2015	Submittal	PCL Project / Job No.
					Check By	TMD	05/05/2015	APPROACH SLABS	I-91 Hartford / 5514001
								Drawing Title	Sheet No.
								APPROACH SLABS 3 & 4	6



**ABUTMENT 1 & 3 APPROACH SLABS  
LOOKING DOWN STATION**



**ABUTMENT 2 & 4 APPROACH SLABS  
LOOKING UPSTATION**

Vermont Agency of Transportation

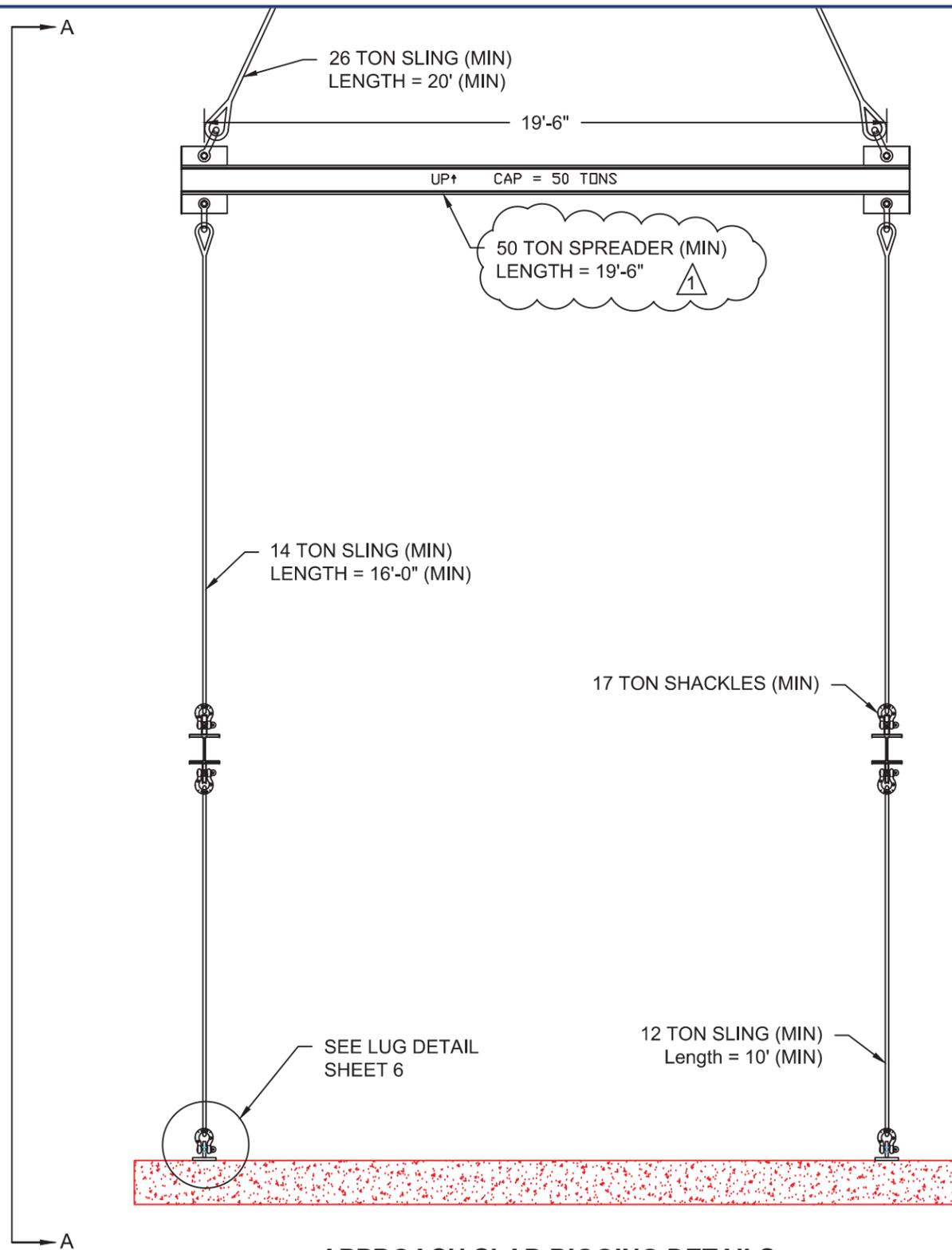
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CK'D BY WL OK'D BY JS

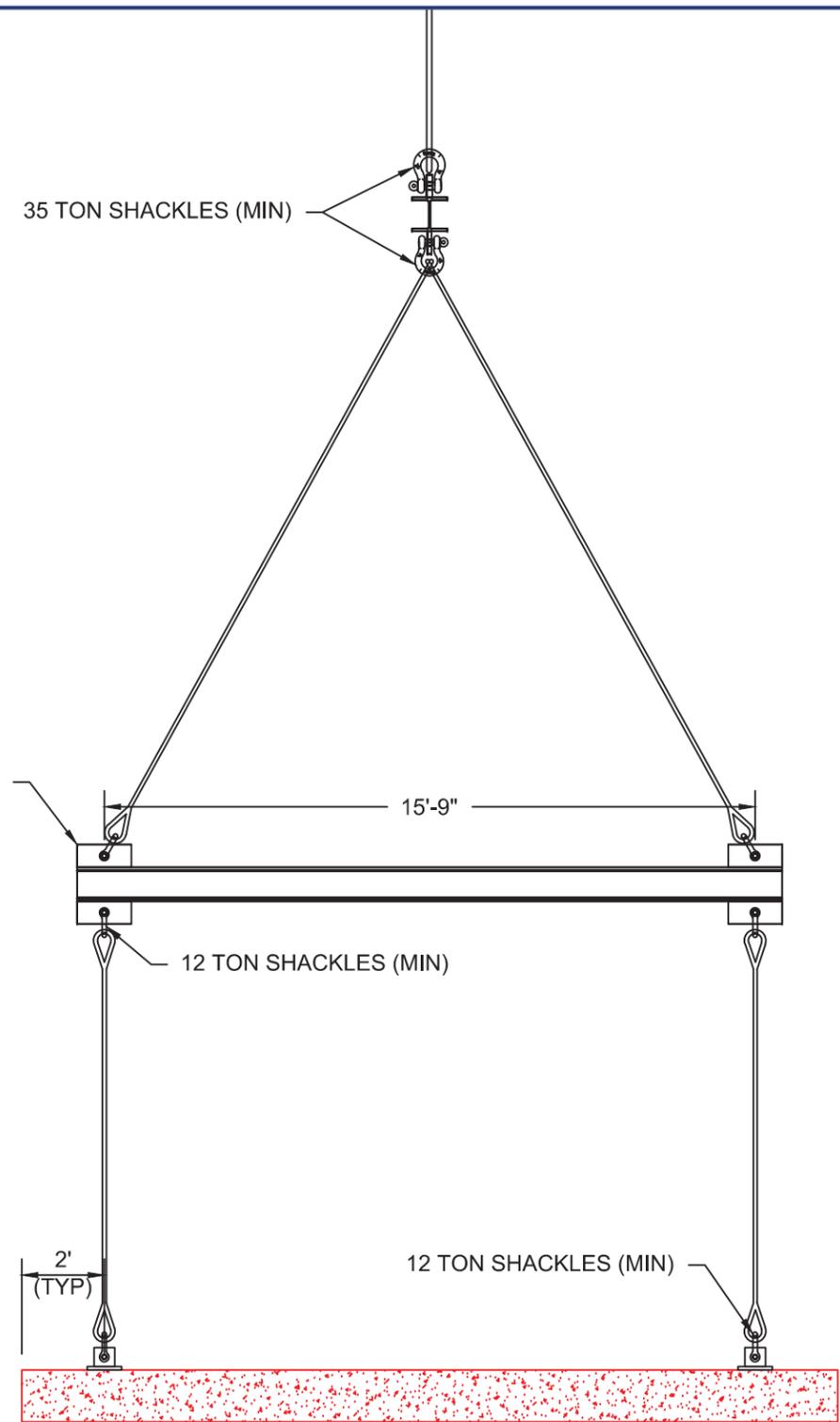
May 28, 2015

RESUBMIT NO Approved                       
BY KH DATE 6-2-2015

Revision No. & Date	Vermont Agency of Transportation				Drawing Status	Name	Date	PCL Civil Constructors, Inc.	
1 5/26/15	Road No.	County / City	Financial Project ID No.		May 27 2015 7:22 PM <b>FOR CONSTRUCTION</b>	Drawn By	EWH	04/13/2015	3810 Northdale Blvd. Suite 200, Tampa Florida 33624 (813)-264-9500 ; Fax: (813)-264-6689
	I-91	Hartford	IM 091-2(79)		Design By	EWH	04/13/2015	Submittal APPROACH SLABS	PCL Project / Job No. I-91 Hartford / 5514001
					Check By	TMD	05/05/2015	Drawing Title POST TENSIONING DUCT DETAILS	Sheet No. 7 



**APPROACH SLAB RIGGING DETAILS**

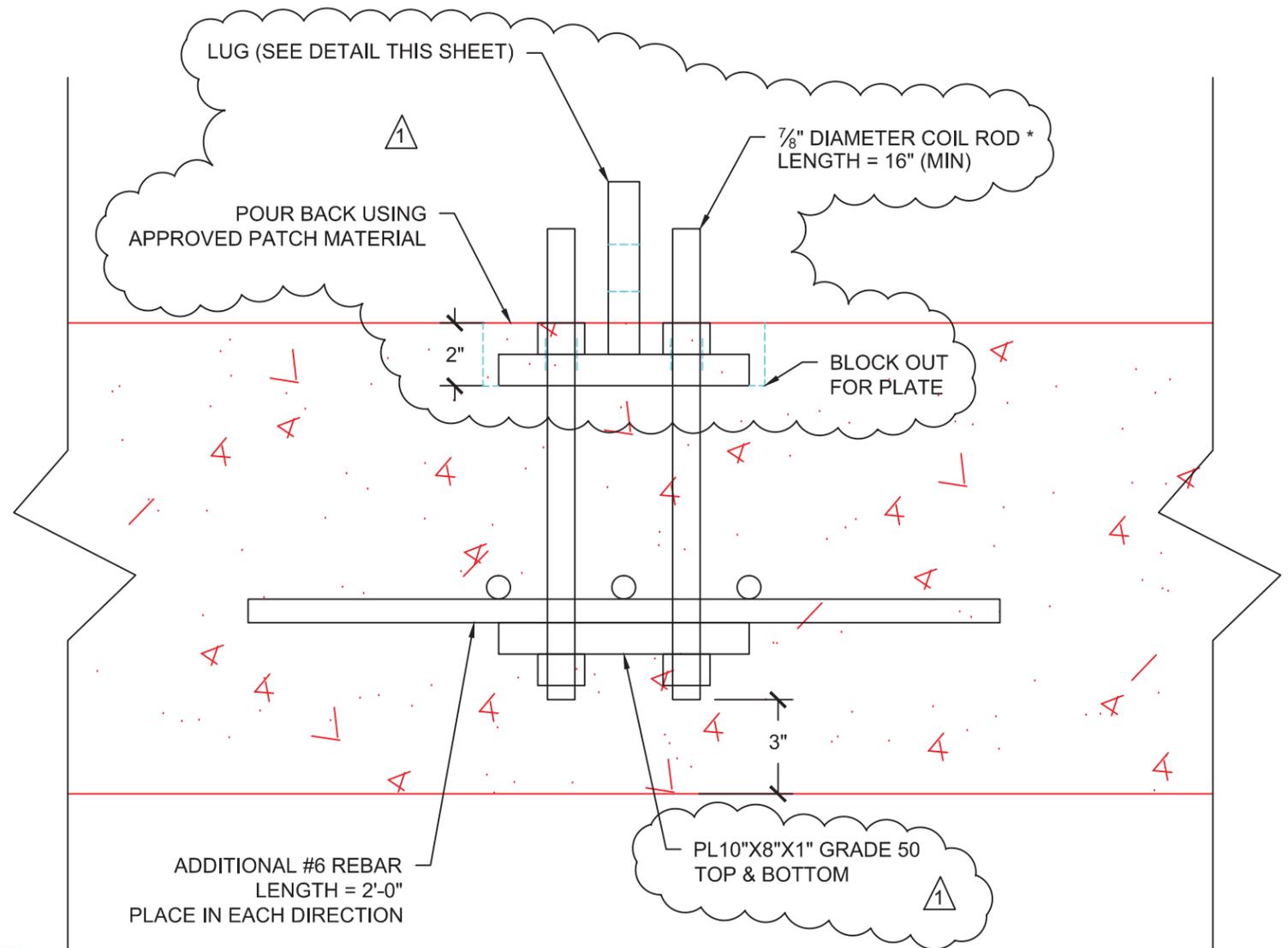
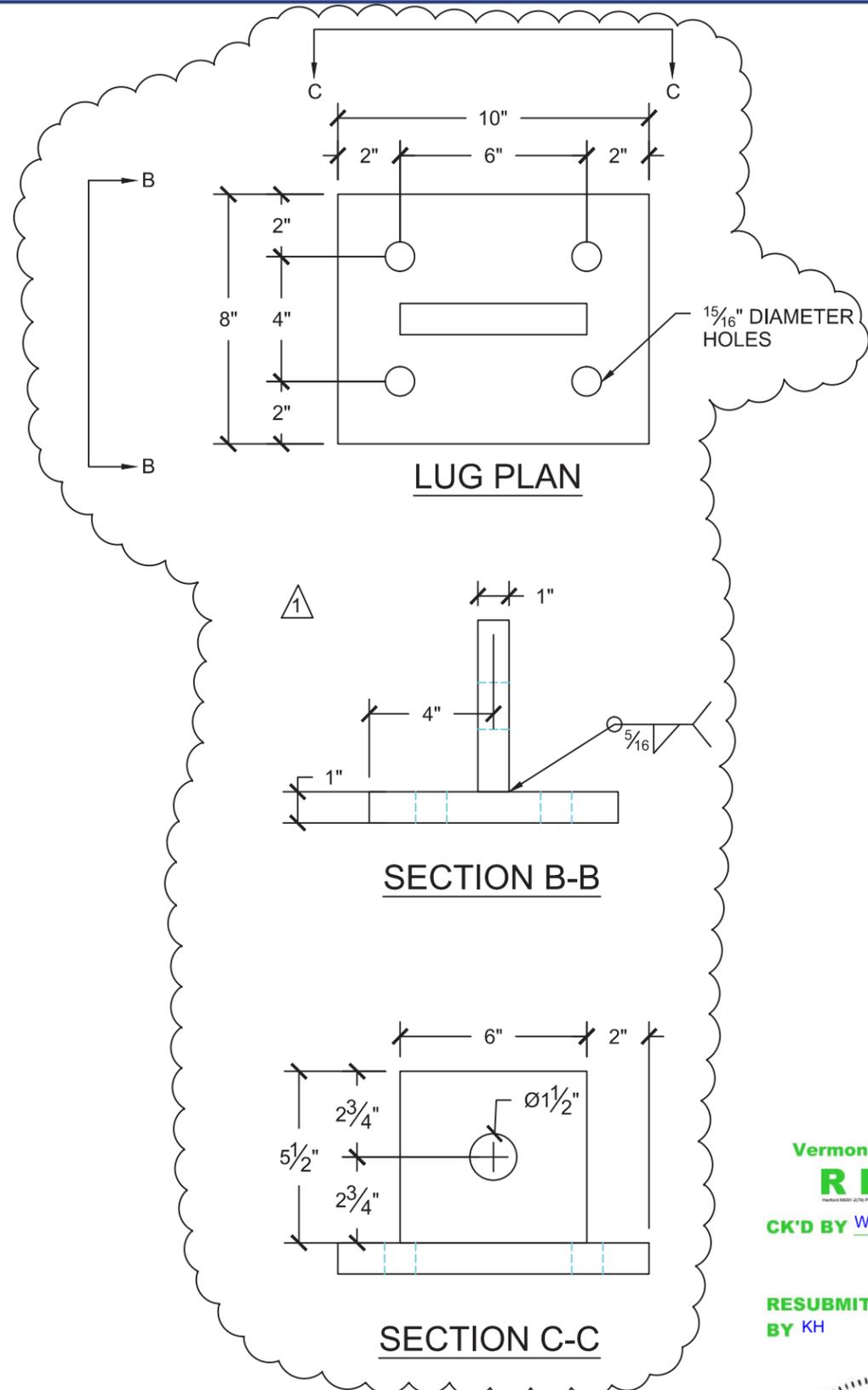


**SECTION A-A**

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1 5/26/15				May 27 2015 7:22 PM	Drawn By	EWH	04/13/2015	3810 Northdale Blvd. Suite 200, Tampa Florida 33624 (813)-264-9500 ; Fax: (813)-264-6689
Road No.	County / City	Financial Project ID No.		FOR CONSTRUCTION	Design By	EWH	04/13/2015	Submittal APPROACH SLABS
I-91	Hartford	IM 091-2(79)		Check By	TMD	05/05/2015	Drawing Title RIGGING DETAILS	PCL Project / Job No. I-91 Hartford / 5514001
								Sheet No. 8



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 BY KH DATE 6-2-2015

**REINFORCEMENT DETAIL**

\* COIL ROD TO BE TORCH CUT FLUSH WITH BLOCKOUT

Revision No. & Date	Vermont Agency of Transportation			Drawing Status	Name	Date	PCL Civil Constructors, Inc.	
1 5/26/15				May 27 2015 7:22 PM	Drawn By EWH	04/13/2015	3810 Northdale Blvd. Suite 200, Tampa Florida 33624 (813)-264-9500 ; Fax: (813)-264-6689	
Road No.	County / City	Financial Project ID No.		FOR CONSTRUCTION	Design By EWH	04/13/2015	Submittal APPROACH SLABS	PCL Project / Job No. I-91 Hartford / 5514001
I-91	Hartford	IM 091-2(79)			Check By TMD	05/05/2015	Drawing Title LIFTING LUG DETAILS	Sheet No. 9



# QUALITY CONTROL PROCESSES

# Approach Slab Quality Control Processes

## 1. Concrete Production

Prior to pouring of the permanent concrete for the approach slabs, concrete leveling slabs will be poured as bases. The approach slabs will be poured on top of a smooth surface.



Prior to concrete placement a pre-production meeting will be held between the Contractor, Resident Engineer and all inspection staff.

Concrete will be supplied by Carroll Concrete. The approved mix design is included for reference. Concrete will be inspected at the plant and again when it arrives on site to ensure that it meets all requirements of the specifications.

VTrans will be responsible for Quality Assurance Testing.

The Contractor will be responsible for making additional cylinders for early breaks. Cylinders will be broken by S.W. Cole Engineering, Inc.

Each approach slab will be marked with its unit number and date of casting.

Approach slabs will be inspected by both the Contractor and the Resident Engineer and documented.

- Minor defects will be repaired using an approved patch material from the VTrans APL. Minor defects are defined as holes, honeycombing, or spalls, which are 6" or less in diameter, that do not penetrate deeper than 1" into the concrete.
- Surface voids or "bugholes" that are less than 5/8" in diameter and less than 1/4" deep are not required to be repaired.
- Cracks less than .01" in width shall be sealed by a method approved by the Engineer. Cracks in excess of .01" may be cause for rejection.

Concrete tolerances: length –  $\pm 1/4$ ", width –  $\pm 1/4$ ", skew/squareness (plan) –  $\pm 1/2$ ", depth –  $\pm 1/4$ "



## 2. Formwork

Prior to pouring concrete all formwork will be inspected by the Contractor and Resident Engineer to ensure that it is installed per plan. Drawings and calculations are included for reference.



Formwork will be thoroughly cleaned and free of extraneous material such as dirt, loose chips, and dust from concrete surface. If compressed air is used, it will be free of oil.

Note: Prior to removal of forms the concrete must achieve 85% of design strength (4,250 PSI). Cure must be maintained for 7 days.



## 3. Reinforcing Steel

Prior to pouring concrete all reinforcing steel will be inspected by the Contractor and Resident Engineer to ensure that it is installed per the approved drawings.

All reinforcing steel will be clean from foreign material.



Reinforcing Steel Tolerances: reinforcing placement –  $\pm 1/4$ ", cover –  $\pm 1/4$ ", bar Spacing –  $\pm 1$ "

Note: All approach slab reinforcing steel shall be Level II or higher.

## 4. Concrete Finishing

The top surface of the approach slabs are to receive a "tined" finish.

Vermont Agency of Transportation

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VERMONT DEPARTMENT OF TRANSPORTATION

CK'D BY JW, CB, JR OK'D BY JS

June 17, 2015

RESUBMIT NO  
BY KH

Approved AsNoted  
DATE 6-18-2015

## 5. Concrete Curing

Curing will take place immediately upon completion of finishing of the top surface. The approach slabs will be wetted and covered with visqueen/burlap for a minimum of 7 days.

## 6. Installation Procedure

The approach slabs will be cast on site in the medians between I-91 NB & I-91 SB. Drawings are included for reference.

Prior to installation, the keyways & surfaces to be bonded will be cleaned to remove any foreign material. 

During the closure weekend, the cranes will pick the approach slabs (one at a time) and walk down the medians back towards the abutments. Calculations for the lifting attachments and analysis of the approach slabs are included.

The cranes will then walk from the medians onto I-91 (NB/SB). Pending on the slope between the medians & I-91 (NB/SB), the approach slabs may need to be set down prior to walking onto the roadway. The cranes will then walk (with the approach slabs) towards the abutments and the approach slabs will be set in their final position.

 Note: Prior to moving the approach slabs the concrete must achieve 28 day design strength (5,000 PSI) and complete 7 day cure.

Note: Prior to setting the approach slabs the surface elevation of the backfill we be checked to ensure that it is level and at proper grade.

Vermont Agency of Transportation

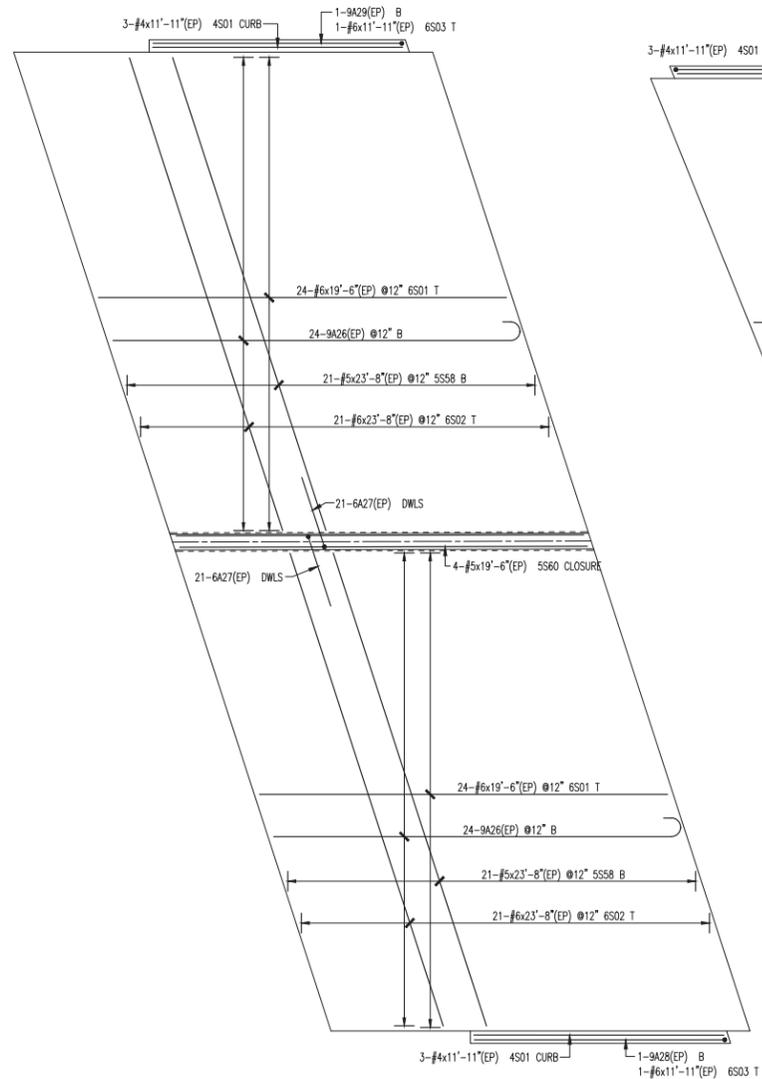
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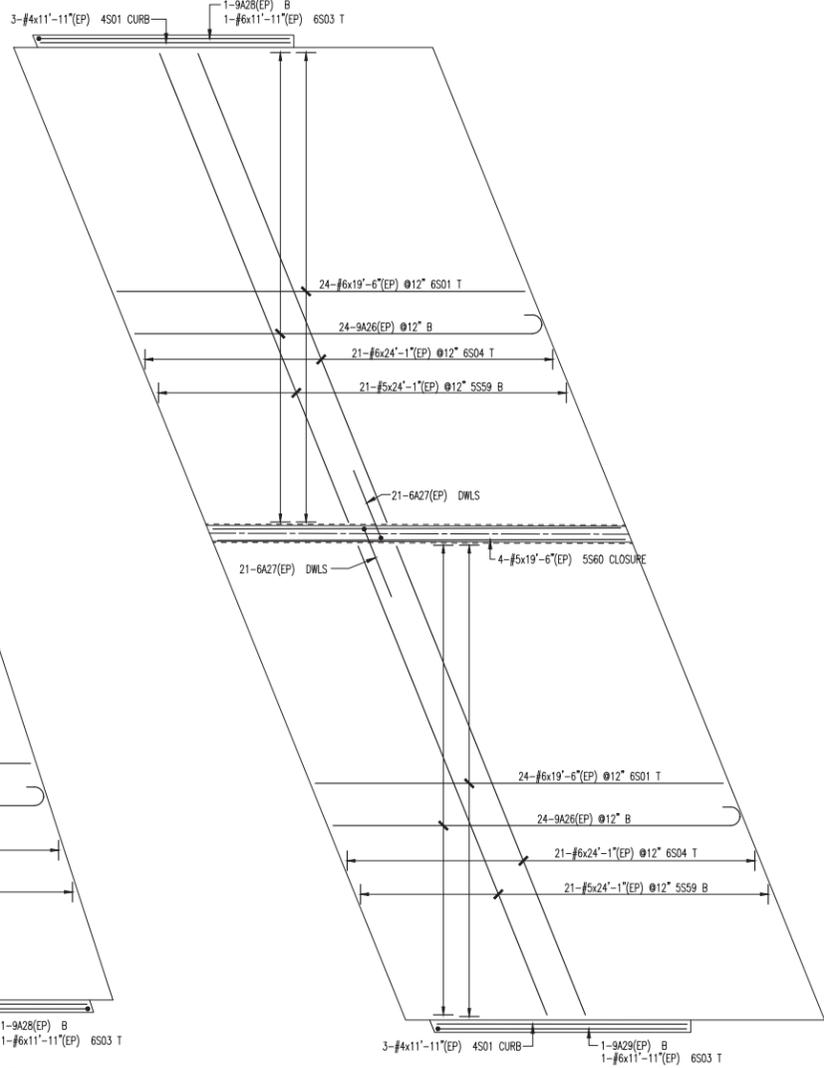
June 17, 2015

RESUBMIT NO Approved AsNoted  
BY KH DATE 6-18-2015

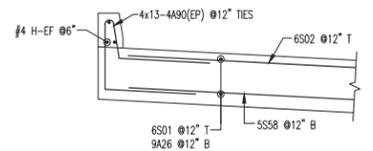
# **APPROVED REINFORCING STEEL DRAWINGS**



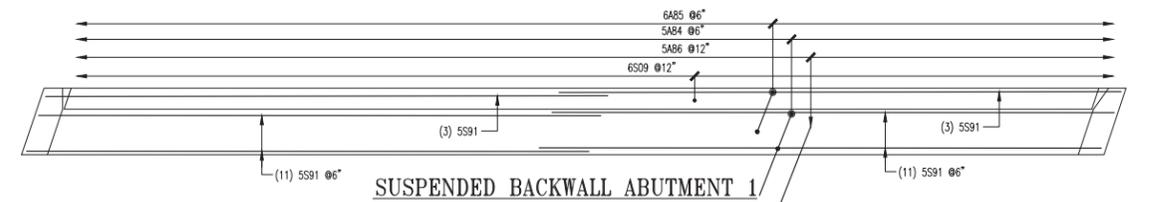
ABUTMENT 1 APPROACH SLAB



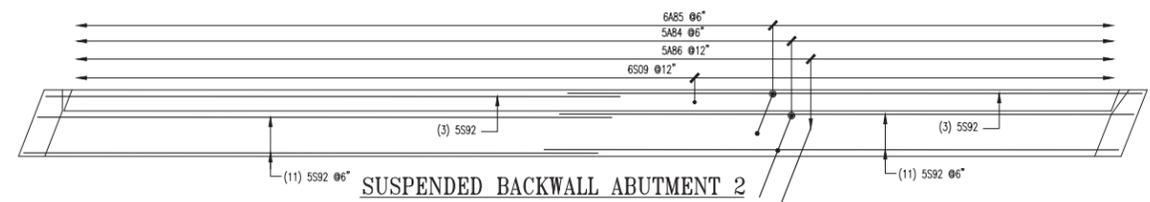
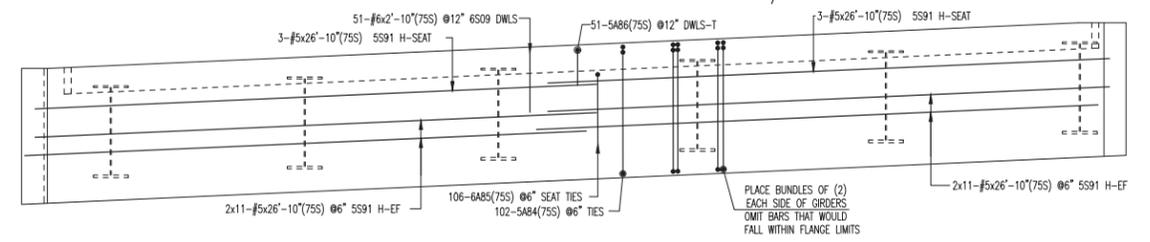
ABUTMENT 2 APPROACH SLAB



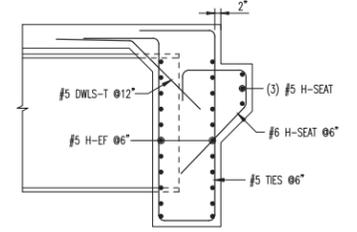
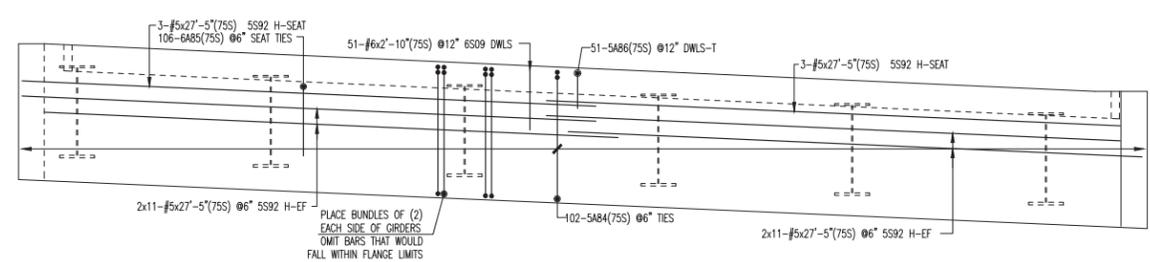
TYPICAL APPROACH SLAB @ CURB



SUSPENDED BACKWALL ABUTMENT 1



SUSPENDED BACKWALL ABUTMENT 2



TYPICAL SUSPENDED BACKWALL SECTION

ALL MATERIAL NOTED AS (75S) SHALL BE "ASTM A955" STAINLESS STEEL

ALL MATERIAL NOTED AS "EP" SHALL BE ASTM A1055 GRADE 60 "DUAL COATED"

SEE SHEET R06S FOR BAR LISTS  
3" CLR COVER UNL.O.

SIZE	TOP BARS	OTHER BARS
#11		
#10		
#9		
#8	54"	54"
#7	41"	41"
#6	31"	31"
#5	26"	26"
#4		
#3		

\* Top bars are horiz. bars with more than 12" of concrete cast below the bars.

Vermont Agency of Transportation  
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March 9, 2015  
RESUBMIT NO Approved  
BY KH DATE 3-12-2015

No.	Description	Date	By
2	FINAL APPROVAL PRINT	03/09/15	CPS
1	APPROVAL PRINT	02/13/15	CPS

Revisions and Issue Record

The full intent and purpose of this drawing is the placing of reinforcing steel bars ONLY. It is NOT to be used as a means of communication between the Architect, Engineer, Contractor or any other Sub-Trades.

THIS DRAWING IS NOT TO BE SCALED.

HarrisRebar  
National Strength. Local Service.

DETAILED AT:  
CANAAH  
NEW HAMPSHIRE

Project: BRIDGE 43 S REPLACEMENT  
I-91 HARTFORD VT

Drawing: I-91 SOUTHBOUND APPROACH SLABS AND SUSPENDED BACKWALLS

Customer: PCL CIVIL CONSTRUCTORS

Engineer: G LAROCHE

Refer to Release:

Date	Drawn	Chkd.	JOB No.	Dwg. No.
02/09/15	CPS		33505535	R05S

W:\csmample\Projects\33505535\Placing Drawings\DWGS\R01S.dwg

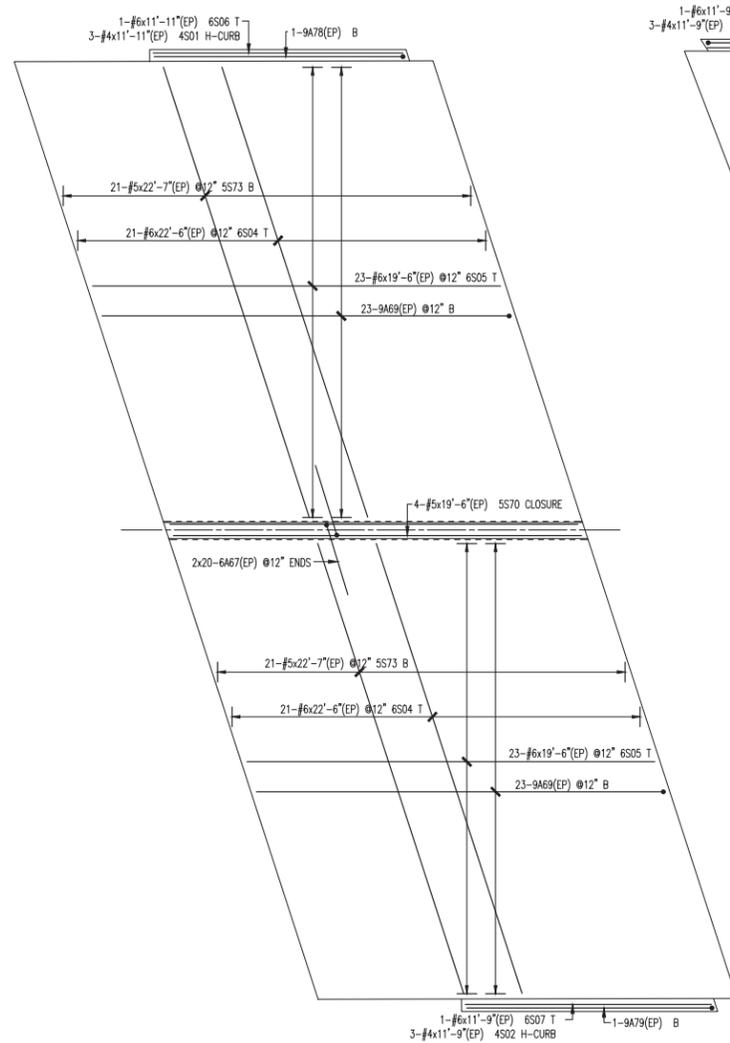
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Bar Mark	Qty	Size	Total Length	Type	X	Y	Z	W	V	U	T	S
Variables To												
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A16b	23	#5	7'-5"	17	2'-5"	2'-7"	2'-5"					
A16c	14	#5	5'-4"	H91	2'-8"	2'-8"						
A16d	2	#5	7'-3"		2'-5"	4'-4"	2'-7"					
A16e	8	#5	12'-5"	3	7'-8"	4'-9"	3'-3"					
A16f	14	#5	6'-5"	17	2'-5"	1'-7"	2'-5"					
A16g	1	#5	11'-8"	3	7'-5"	3'-7"						
A16h	1	#5	7'-11"	3	7'-5"	5"						
A16i	22	#5	4'-10"	3	2'-5"	2'-5"						
A16j	7	#5	8'-5"		5'-7"							
A16k	2	#5	3'-11"		3'-11"							
A16l	12	#5	9'-7"		9'-7"							
A16m	11	#5	3'-1"		3'-1"							
A16n	7	#5	7'-4"		7'-4"							
A16o	1	#5	5'-6"		5'-6"							
A16p	1	#5	8'-5"		8'-5"							
A16q	14	#5	7'-10"		7'-10"							
A16r	11	#5	5'-7"		5'-7"							
A16s	23	#5	7'-0"		7'-0"							
A16t	7	#5	5'-5"		5'-5"							
A16u	1	#5	5'-8"		5'-8"							
A16v	7	#5	10'-5"		10'-5"							
A16w	1	#5	6'-11"		6'-11"							
A16x	101	#5	7'-5"	17	2'-5"	2'-7"	2'-5"					
A16y	26	#5	5'-4"	H91	2'-8"	2'-8"						
A16z	28	#5	4'-10"	3	2'-5"	2'-5"						
A16aa	58	#5	11'-0"	3	5'-6"	5'-6"						
A16ab	14	#5	12'-11"	16	4'-7"	1'-7"	4'-9"					
A16ac	76	#5	8'-4"	25	1'-4"	2'-3"	10"	2'-3"	1'-4"			
A16ad	24	#5	8'-4"		9'-8"							
A16ae	24	#5	15'-1"		15'-1"							
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A16bc	11	#7	11'-0"		11'-0"							
A16bd	37	#7	14'-1"		14'-1"							
A16be	23	#7	19'-8"		19'-8"							
A16bf	218	#7	10'-6"		10'-6"							
A16bg	43	#7	12'-10"		12'-10"							
A16bh	23	#8	14'-3"	17	5'-4"	8'-9"						
A16bi	80	#9	14'-4"	17	5'-7"	8'-9"						
A16bj	80	#9	10'-0"		10'-0"							
A16bk	1	#5	1'-11"		1'-11"							
A16bl	1	#5	5'-1"		5'-1"							
A16bm	3	#5	7'-4"		7'-4"							
A16bn	1	#5	4'-8"		4'-8"							
A16bo	26	#5	15'-5"	3	2'-5"	6'-7"	2'-5"				1'-11"	1'-4"
A16bp	1	#5	7'-4"		7'-4"							
A16bq	1	#5	4'-8"		4'-8"							

ABUTMENT 1 AND WINGWALLS 1 & 2

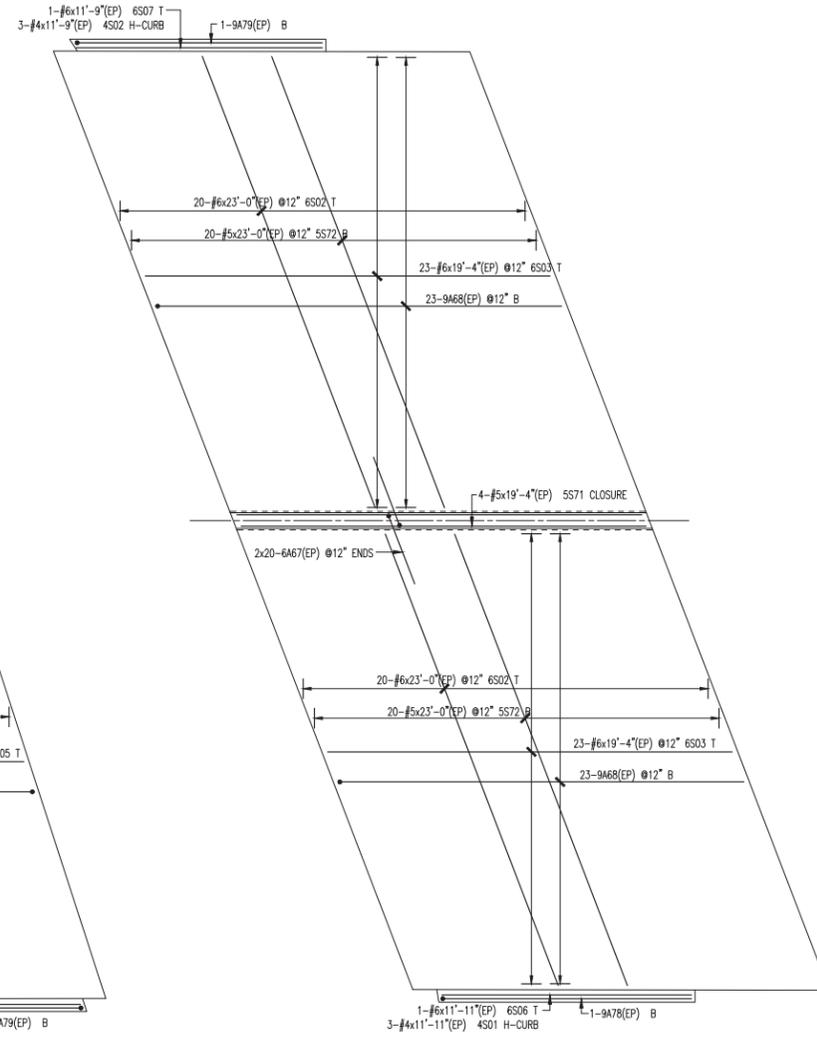
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Variables To												
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A302	204	#5	18'-7"	H66	2'-5"	6'-1"	1'-10"	5'-10"	2'-5"			3"
A303	546	102	5'-6"	3	3'-1"	2'-5"				1'-8"		1'-8"
A304	42	#5	25'-8"		24'-1"							
A305	42	#5	24'-1"		24'-1"							
A306	8	#5	19'-4"		19'-4"							
A307	50	#5	26'-10"		26'-10"							
A308	50	#5	27'-5"		27'-5"							
A309	84	#6	7'-3"	S11	7'-3"					3'-6"		7"
A310	685	212	7'-3"	16	7'-1"	1'-2"	3'-0"			2'-1"		3'-3"
A311	86	#6	19'-4"		19'-4"							
A312	43	#6	25'-8"		25'-8"							
A313	4	#6	11'-11"		11'-11"							
A314	42	#6	24'-1"		24'-1"							
A315	639	102	2'-10"		2'-10"							
A316	96	#9	20'-8"	1	1'-3"	19'-5"						11"
A317	2	#9	15'-3"	1	1'-3"	12'-0"						11"
A318	2	#9	15'-2"	1	1'-3"	11'-11"						11"
A319	52	#4	7'-0"	H1	2'-2"	1'-6"	3"	10"	2'-2"			

APPROACH SLABS & SUSPENDED BACKWALLS

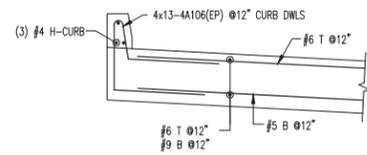
Drawing Sheet : R015												
Bar Mark	Qty	Size	Total Length	Type	X	Y	Z	W	V	U	T	S
Variables To												
A425	462	#4	5'-0"	1	5'-0"							
A426	4	#5	5'-8"	17	2'-7"							
A427	4	#5	7'-6"	17	2'-5"							
A428	10	#5	6'-5"		6'-5"							
A429	10	#5	9'-1"		9'-1"							
A430	1	#5	2'-5"		2'-5"							
A431	1	#5	28'-6"		28'-6"							
A432	2	#5	11'-9"		11'-9"							
A433	2	#5	19'-1"		19'-1"							
A434	1	#5	1'-6"		1'-6"							
A435	1	#5	27'-8"		27'-8"							
A436	2	#5	18'-7"		18'-7"							
A437	2	#5	25'-11"		25'-11"							
A438	480	#5	3'-9"	1	7"	3'-2"						
A439	378	#5	4'-10"	H1	1'-3"	8"	1'-1"	6"	1'-3"			5"
A440	418	#5	7'-9"	H2	10"	2'-9"	1'-2"	2'-11"	2'-11"			2"
A441	76	#5	9'-7"	H3	1'-6"	3'-2"	5"	2'-11"	1'-6"			5"
A442	123	#5	5'-8"	1	7"	5'-1"						
A443	89	#5	24'-4"		24'-4"							
A444	8	#5	24'-8"		24'-8"							
A445	388	#5	30'-0"		30'-0"							
A446	6	#5	11'-6"		11'-6"							
A447	6	#5	20'-2"		20'-2"							
A448	6	#5	20'-7"		20'-7"							
A449	6	#5	11'-9"		11'-9"							
A450	6	#5	11'-0"		11'-0"							
A451	1	#6	2'-8"		2'-8"							
A452	1	#6	2'-8"		2'-8"							
A453	1	#6	21'-11"		21'-11"							
A454	1	#6	2'-5"		2'-5"							
A455	1	#6	26'-10"		26'-10"							
A456	1	#6	1'-6"		1'-6"							
A457	1	#6	27'-8"		27'-8"							
A458	1	#6	3'-6"		3'-6"							
A459	1	#6	22'-10"		22'-10"							
A460	56	#6	30'-0"		30'-0"							
A461	14	#6	26'-4"		26'-4"							
A462	504	#6	25'-7"		25'-7"							
A463	32	#7	14'-4"									



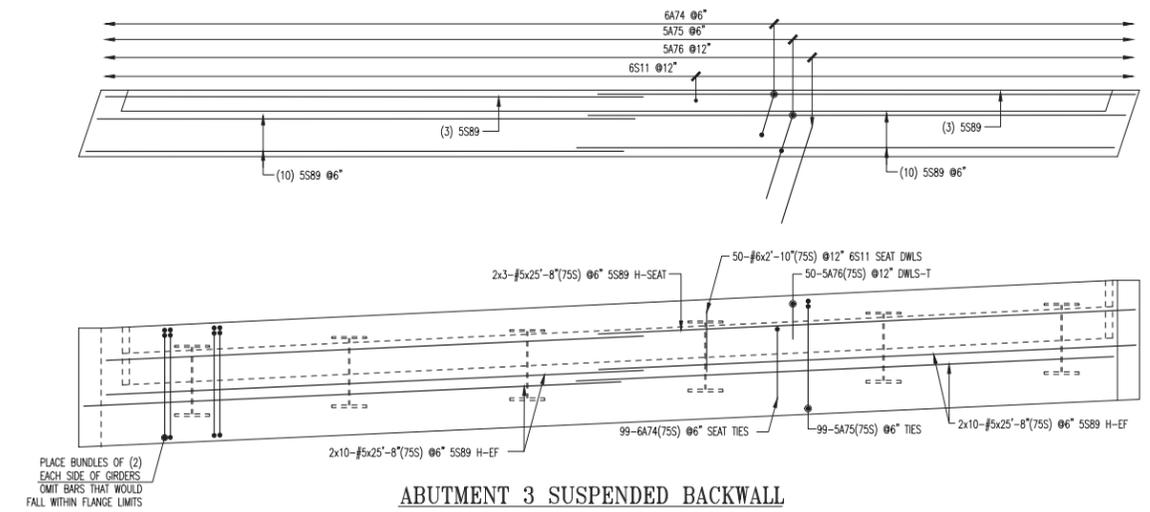
ABUTMENT 3 APPROACH SLAB



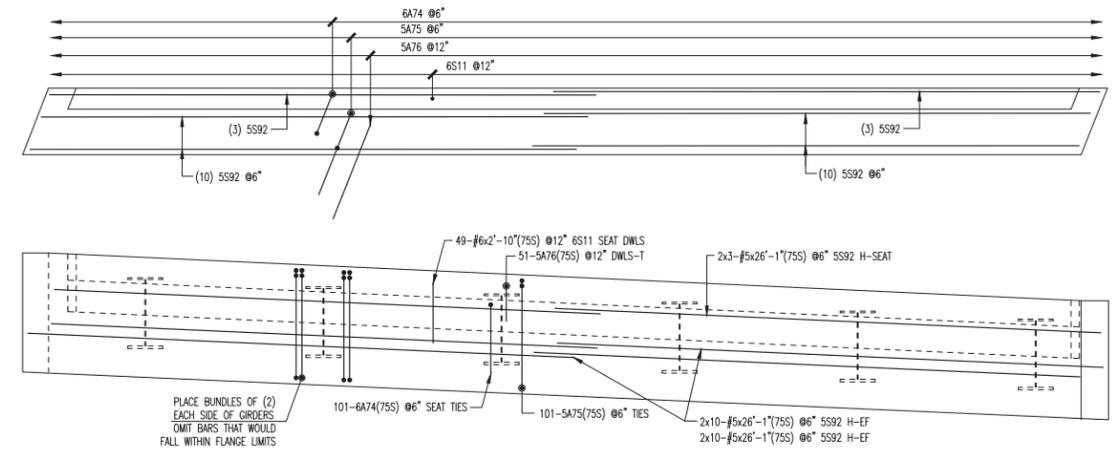
ABUTMENT 4 APPROACH SLAB



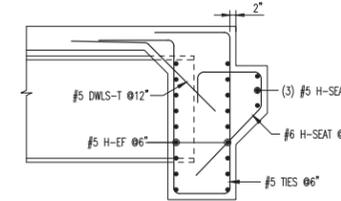
TYPICAL APPROACH SLAB @ CURB



ABUTMENT 3 SUSPENDED BACKWALL



ABUTMENT 4 SUSPENDED BACKWALL



TYPICAL SUSPENDED BACKWALL SECTION

SEE SHEET R06S FOR BAR LISTS  
3" CLR COVER UNL.D.

LAP CHART-U.N.O.

SIZE	TOP BARS *	OTHER BARS
#11		
#10		
#9		
#8	54"	54"
#7	44"	44"
#6	34"	34"
#5	24"	24"
#4		
#3		

\* Top bars are horiz. Bars with more than 12" of concrete cast below the bars.

Vermont Agency of Transportation  
**RECEIVED**  
CK'D BY RK/GL OK'D BY WL  
March 9, 2015  
RESUBMIT NO Approved  
BY KH DATE 3-12-2015

ALL MATERIAL ON THIS DRAWING NOTED AS (75S) SHALL BE ASTM A955 STAINLESS STEEL

ALL MATERIAL ON THIS DRAWING NOTED AS (EP) SHALL BE ASTM A1055 GR60 "DUAL COATED" REINF.

No.	Description	Date	By
2	FINAL APPROVAL PRINT	03/09/15	CPS
1	APPROVAL PRINT	02/18/15	CPS

Revisions and Issue Record

The full intent and purpose of this drawing is the placing of reinforcing steel bars ONLY. It is NOT to be used as a means of communication between the Architect, Engineer, Contractor or any other Sub-trades.

THIS DRAWING IS NOT TO BE SCALED.

HarrisRebar  
National Strength. Local Service.

Project: HARTFORD LATERAL BRIDGE I-91 NORTHBOUND  
Drawing: APPROACH SLABS AND BACKWALLS REINF.  
Customer: PCL CIVIL CONSTRUCTORS  
Engineer: G. LAROCHE  
Refer to Release:

Date	Drawn	Chkd.	JOB No.	Dwg. No.
02/10/15	CPS		33505535	R05N

W:\sample\Projects\33505535\Placing Drawings\DWGS\R01N.dwg



# **APPROVED CONCRETE MIX DESIGN**

