

Erection Plan Support Calculations
BF-013-4(39)

Waitsfield, Vermont

CEE 36-mi-16



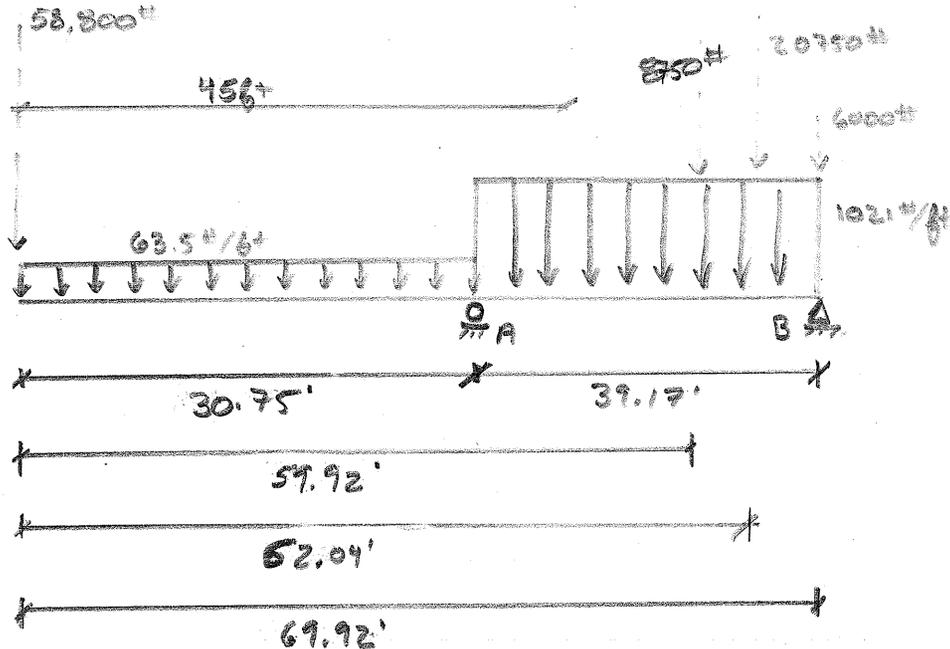
Prepared for:
A.L. St Onge Contractor, Inc

By:
Calderwood Engineering
June 6th, 2015

COUNTER WEIGHTS: 6000 lbs @ 84.92'
 20750 lbs @ 77.04'
 8750 lbs @ 74.92'
 HL-1507 : 1.021 K/lft
 BOOM : 63.5 K/lft

NOTE: HL-1507 w/
 150ft boom
 IS RATED FOR
 66,900 lb @
 RADIUS 45ft

WORST LOAD CASE : MAX RADIUS : 45ft
 LOAD : 58,800 lb



SUPPORT A : 134000 lb ← CONTROLS * CALCS DONE ON BEAM BOY
 SUPPORT B : 2140 lb

P = 134 K SEE PAGE 10

CHECK CRANE MAT CAPACITY FOR HL-1507 LOADED @ MAX RADIUS

ASSUMPTIONS & KNOWNS

- USE CRANE MATS TO DISTRIBUTE LOAD
- ASSUME (4) 4' x 12' x 8" CRANE MATS STACKED
- MOST LOADED OUTRIGGER: $P = 134k$ FROM BEAMBOY

$$(D) \text{ DEPTH: } 2'8''$$

$$(B) \text{ BASE: } 4'$$

$$(L) \text{ LENGTH: } 12'$$

$$\gamma_{\text{wood}} = 50 \text{ pcf DENSE HARDWOOD}$$

$$W_{\text{allow}} = 5 \text{ ksi} \rightarrow \text{STANDARD SPECIFICATIONS FOR HIGHWAY BRIDGES TABLE 4.11.4.1.4-1}$$

$$\begin{aligned} P_{\text{dead}} &= D \cdot B \cdot L \cdot \gamma_{\text{wood}} \\ &= (2'8'') (4') (12') (50 \text{ pcf}) \\ &= 6.4 \text{ kip} \end{aligned}$$

$$w = \frac{(P + P_{\text{dead}})}{(L \cdot B)} = \frac{(134k + 6.4k)}{(12' \cdot 4')} = 2.925 \text{ ksi}$$

$$FS: \frac{W_{\text{allow}}}{w} = \frac{5 \text{ ksi}}{2.925 \text{ ksi}} = 1.62 \text{ OK} \checkmark$$

CHECK CRANE MAT MOMENT CAPACITY

MODEL AS A CANTILEVER SUPPORT @ CENTER OF CRANE MAT
ANALYZE ON A PER FOOT BASIS

$$\begin{aligned} M_B &= w \cdot \frac{L}{2} \cdot \left(\frac{\frac{L}{2}}{2} \right) \cdot 16' \\ &= (2.925 \text{ ksi}) \cdot \left(\frac{12'}{2} \right) \cdot \left(\frac{12'/2}{2} \right) \cdot 16' \\ &= 52.65 \text{ ft} \cdot \text{k} \\ M_B &= 631.8 \text{ in} \cdot \text{k} \end{aligned}$$

→ NDS

CALCULATE CAPACITY (REF NATIONAL DESIGN SPECIFICATIONS FOR WOOD CONSTRUCTION)

$$F_b = 1150 \text{ psi} \leftarrow \text{MIXED OAK No. 1, NDS SUPPLEMENT TABLE 4D}$$

$$C_D = 1.25 \leftarrow \text{NDS TABLE 2.3.2 FOR CONSTRUCTION LOADS}$$

$$C_M = 1.0$$

$$C_t = 1.0 \leftarrow \text{NDS TABLE 2.3.3}$$

$$C_L = 1.0 \leftarrow \text{NDS 3.3.3}$$

$$C_F = 1.0 \leftarrow \text{NDS 4.3.6}$$

$$C_{Fu} = 1.0$$

$$C_i = 1.0$$

$$C_r = 1.0$$

$$F'_b = F_b \cdot C_D \cdot C_M \cdot C_t \cdot C_L \cdot C_F \cdot C_r$$

$$F'_b = (1150 \text{ psi}) (1.25)$$

$$F'_b = 1437.5 \text{ psi}$$

NEXT PAGE ⇒

$$B = 16t \quad \leftarrow \text{B/C ANALYZING ON PER FOOT BASIS}$$

$$H = 8''$$

$$S_x = 4 \cdot \frac{BH^2}{6} \quad (4) \text{ MATS STACKED ON TOP OF EACH OTHER}$$

$$= 4 \frac{(16t)(.667t)^2}{6}$$

$$S_x = .2168t^3 = 511.5 \text{ in}^3$$

$$M_y = S_x \cdot F/b$$

$$M_y = (511.5 \text{ in}^3)(1437.5 \text{ psi})$$

$$M_y = 735.264 \text{ K.in}$$

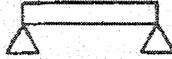
$$FS = \frac{M_y}{M} = \frac{735.264 \text{ K.in}}{667.49 \text{ K.in}} = 1.1 \quad \text{OK} \checkmark$$

USE (4) 4'x12'x8" CRANE
MATS

Grove HL 150

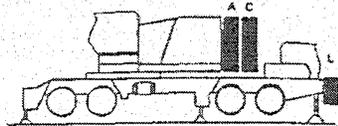
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76A BOOM - ON OUTRIGGERS 360°
85% STABILITY



CAPACITY IN POUNDS
WITH A C + L COUNTERWEIGHTS

BOOM LGTH	LOAD RAD	BOOM ANG	SHEAVE HGT	RATED LOAD
40	12	82.7	47.1	300,000
40	13	81.3	46.9	294,600
40	14	79.8	46.6	272,900
40	15	78.3	46.3	254,300
40	16	76.8	46.0	237,800
40	17	75.3	45.7	223,400
40	18	73.8	45.3	210,500
40	19	72.2	44.9	199,100
40	20	70.7	44.5	188,700
40	25	62.6	41.8	149,300
40	30	53.7	38.1	122,900
40	35	43.4	32.9	99,500
40	40	29.9	24.9	81,000
50	13	83.0	57.0	293,800
50	14	81.9	56.9	272,100
50	15	80.7	56.6	253,500
50	16	79.5	56.4	237,000
50	17	78.3	56.1	222,600
50	18	77.1	55.8	209,700
50	19	75.9	55.5	198,300
50	20	74.7	55.2	187,900
50	25	68.6	53.2	148,500
50	30	62.1	50.5	122,200
50	35	55.1	46.9	99,700
50	40	47.3	42.4	81,100
50	45	38.2	36.2	67,900
50	50	26.2	27.0	58,000
60	15	82.3	66.8	253,100
60	16	81.3	66.6	236,600
60	17	80.3	66.4	222,300
60	18	79.3	66.2	209,300
60	19	78.4	65.9	197,900
60	20	77.4	65.7	187,500
60	25	72.3	64.0	148,100
60	30	67.2	61.8	121,900
60	35	61.7	59.1	99,900
60	40	55.9	55.7	81,300
60	45	49.7	51.5	68,100
60	50	42.7	46.1	58,300
60	60	23.6	28.8	44,500
70	17	81.7	76.6	222,000
70	18	80.9	76.4	209,100
70	19	80.1	76.2	197,700
70	20	79.2	76.0	187,300
70	25	75.0	74.6	147,900
70	30	70.6	72.8	121,700
70	35	66.1	70.5	100,000
70	40	61.5	67.8	81,400
70	45	56.6	64.4	68,200
70	50	51.3	60.4	58,400
70	60	39.2	49.5	44,700
70	70	21.6	30.5	35,500



COUNTERWEIGHT CONFIGURATION

BOOM LGTH	LOAD RAD	BOOM ANG	SHEAVE HGT	RATED LOAD
80	12	82.0	86.6	208,600
80	13	81.3	86.4	197,200
80	20	80.6	86.2	186,800
80	25	76.9	85.8	147,400
80	30	73.2	83.4	121,200
80	35	69.3	81.5	100,000
80	40	65.4	79.2	81,300
80	45	61.3	76.4	68,100
80	50	57.0	73.1	58,300
80	60	47.7	64.7	44,600
80	70	36.4	52.7	35,400
80	80	20.0	32.1	24,200
90	19	82.3	96.6	197,000
90	20	81.6	96.4	186,600
90	25	78.4	95.3	147,400
90	30	75.1	93.9	121,100
90	35	71.7	92.3	100,000
90	40	68.3	90.2	81,400
90	45	64.8	87.8	68,100
90	50	61.1	85.1	58,400
90	60	53.4	78.1	44,700
90	70	44.7	68.8	35,600
90	80	34.2	55.7	29,200
90	90	18.7	33.6	24,200
100	21	81.9	106.4	176,900
100	25	79.6	105.6	147,000
100	30	76.6	104.3	120,600
100	35	73.6	102.8	100,000
100	40	70.6	101.1	81,300
100	45	67.5	98.9	68,000
100	50	64.3	96.5	58,200
100	60	57.6	90.5	44,400
100	70	50.4	82.8	35,300
100	80	42.2	72.5	29,000
100	90	32.3	58.5	24,100
100	100	17.6	35.0	20,200
110	24	81.1	116.0	152,900
110	25	80.5	115.8	146,500
110	30	77.9	114.7	120,200
110	35	75.2	113.3	99,800
110	40	72.4	111.7	81,100
110	45	69.7	109.8	67,800
110	50	66.8	107.7	58,000
110	60	60.9	102.4	44,200
110	70	54.7	95.7	35,100
110	80	47.8	87.1	28,800
110	90	40.1	76.1	23,900
110	100	30.6	61.1	20,100
110	110	16.7	36.3	17,000
120	26	80.8	125.8	139,900
120	30	78.9	124.9	119,600
120	35	76.4	123.7	99,700
120	40	74.0	122.2	81,000
120	45	71.4	120.5	67,600
120	50	68.9	118.6	57,800
120	60	63.6	113.8	44,000
120	70	58.0	107.9	34,800
120	80	52.1	100.5	28,500
120	90	45.6	91.3	23,600
120	100	38.2	79.5	19,800
120	110	29.2	63.6	16,700
120	120	15.9	37.6	14,200
130	27	81.1	135.8	134,000
130	30	79.8	135.2	119,300
130	35	77.5	134.0	99,500
130	40	75.2	132.7	80,800
130	45	72.9	131.1	67,400
130	50	70.6	129.3	57,600
130	60	65.8	125.0	43,800
130	70	60.8	119.7	34,700
130	80	55.5	113.1	28,300
130	90	49.9	105.1	23,500
130	100	43.7	95.2	19,700
130	110	36.6	82.7	16,700
130	120	28.0	66.0	14,200
130	130	15.2	38.8	12,000
140	29	80.9	145.5	123,400
140	30	80.5	145.4	118,800
140	35	78.4	144.3	99,400
140	40	76.3	143.1	80,600
140	45	74.2	141.6	67,200
140	50	72.0	140.0	57,400
140	60	67.6	136.0	43,500
140	70	63.1	131.2	34,400
140	80	58.3	125.2	28,000
140	90	53.3	118.1	23,100
140	100	47.9	109.5	19,400
140	110	42.0	99.0	16,300
140	120	35.2	85.8	13,800
140	130	26.9	68.3	11,700
140	140	14.6	40.0	10,000
150	30	81.1	155.5	118,300
150	35	79.2	154.5	99,200
150	40	77.2	153.4	80,400
150	45	75.3	152.1	66,900
150	50	73.3	150.5	57,100
150	60	69.2	146.9	43,200
150	70	65.0	142.4	34,100
150	80	60.7	137.0	27,700
150	90	56.1	130.5	22,900
150	100	51.3	122.9	19,100
150	110	46.1	113.7	16,000
150	120	40.4	102.6	13,500
150	130	33.9	88.8	11,500
150	140	26.0	70.5	9,700
150	150	14.1	41.1	8,200

RATED LOADS APPEARING IN SHADED AREAS ARE BASED ON STRUCTURAL OR OTHER FACTORS RATHER THAN STABILITY.

READ AND UNDERSTAND LIFTING CAPACITY NOTES ON A6-829-800214 LOCATED IN THE FRONT OF THIS MANUAL BEFORE OPERATING THIS MACHINE.

SERIAL NUMBER

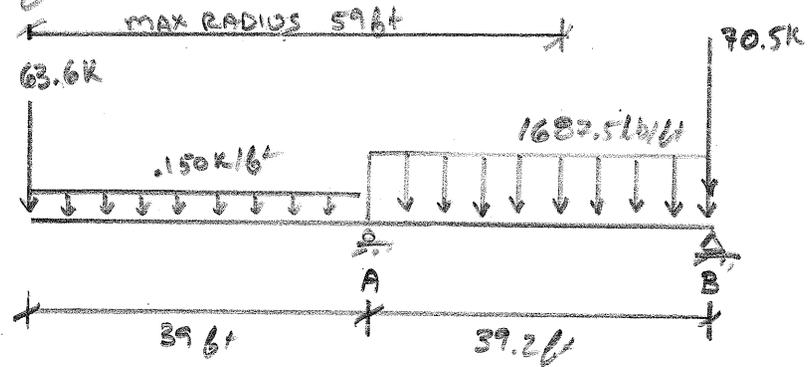
HL150T
IDENTIFICATION

DEMAG AC180

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COUNTER WEIGHT: $141\text{K} / 2 = 70.5\text{K}$
 CRANE: $\frac{132,300\text{Lb}}{39.2\text{ft}} \cdot \frac{1}{2} = 1687.5\text{ lb/ft}$
 BOOM: 150 lb/ft

WORST LOAD CASE:
 MAX RADIUS: 59ft
 LOAD: 63.6K



SUPPORT A: 169000Lb
 SUPPORT B: 37400Lb

P = 169K ✓ SEE PAGE 11

NOTE: DEMAG AC180 w/
 93.1ft BOOM IS
 RATED FOR A
 LOAD OF 65K @ 59'

CHECK CRANE MAT CAPACITY FOR DEMAG AC180 LOADED @ MAX RADIUS ASSUMPTIONS & KNOWN

- USE CRANE MATS TO DISTRIBUTE LOAD
- ASSUME (5) 4'x12'x8" CRANE MATS STACKED
- MOST LOADED OUTRIGGER: P = 169K FROM BEAMBOY

(D) DEPTH: 3'4"
 (B) BASE: 4'
 (L) LENGTH: 12'

$\delta_{\text{WOOD}} = 50\text{pcf} \rightarrow$ DENSE HARDWOOD
 $\text{WALLOW} = 5\text{ksf} \rightarrow$ STANDARD SPECIFICATIONS
 FOR HIGHWAY BRIDGES
 TABLE 4.11.4.1.4-1

$$P_{\text{DEAD}} = (D \cdot B \cdot L) \delta_{\text{WOOD}}$$

$$= (3'4" \cdot 4' \cdot 12') (50\text{pcf})$$

$$= 8000\text{lbs}$$

$$w = \frac{(P + P_{\text{DEAD}})}{(L \cdot B)}$$

$$= \frac{(169\text{K} + 8000\text{lb})}{(12' \cdot 4')}$$

$$= 3.6875\text{ksf}$$

$$F.S. = \frac{\text{WALLOW}}{w} = \frac{5\text{ksf}}{3.7\text{ksf}} = 1.36 \text{ OK } \checkmark$$

42-381 50 SHEETS (EYE/ASE) - 5 SQUARES
 42-382 100 SHEETS (EYE/ASE) - 5 SQUARES
 42-383 200 SHEETS (EYE/ASE) - 5 SQUARES
 National Brand

CHECK CRANE MAT MOMENT CAPACITY

MODEL AS A CANTILEVER SUPPORT @ CENTER OF CRANE MAT
ANALYZE ON A PER FOOT BASIS

$$M_B = w \cdot \frac{L}{2} \cdot \left(\frac{\frac{L}{2}}{2}\right) \cdot 1ft$$

$$M_B = (3.6875 \text{ ksf}) \cdot \left(\frac{12ft}{2}\right) \cdot \left(\frac{\frac{12ft}{2}}{2}\right) \cdot 1ft$$

$$M_B = 796.5 \text{ in} \cdot \text{K}$$

← NDS

CALCULATE CAPACITY (REF NATIONAL DESIGN SPECIFICATIONS FOR WOOD CONSTRUCTION)

$$F_b = 1150 \text{ psi} \quad \leftarrow \text{MIXED OAK No. 1 NDS SUPPLEMENT TABLE 4D}$$

$$C_D = 1.25 \quad \leftarrow \text{NDS TABLE 2.3.2 FOR CONSTRUCTION LOADS}$$

$$C_M = 1.0$$

$$C_t = 1.0 \quad \leftarrow \text{NDS TABLE 2.3.3}$$

$$C_L = 1.0$$

$$C_F = 1.0$$

$$C_{fu} = 1.0$$

$$C_i = 1.0$$

$$C_r = 1.0$$

$$F'_b = F_b \cdot C_D \cdot C_M \cdot C_t \cdot C_L \cdot C_F \cdot C_r$$

$$F'_b = (1150 \text{ psi})(1.25)$$

$$F'_b = 1437.5 \text{ psi}$$

$$B = 1ft \quad \leftarrow \text{BIG ANALYZING ON PER FOOT BASIS}$$

$$H = 8"$$

$$S_x = 5 \cdot \frac{BH^2}{6} = 5 \cdot \frac{(1)(8")^2}{6} = .37 \text{ ft}^3$$

$$M_y = S_x \cdot F'_b$$

$$M_y = (.37 \text{ ft}^3)(1437.5 \text{ psi})$$

$$M_y = 920 \text{ in} \cdot \text{K}$$

$$FS = \frac{M_y}{M_B} = \frac{920 \text{ in} \cdot \text{K}}{796.5 \text{ in} \cdot \text{K}} = 1.16 \text{ OK} \checkmark$$

USE (5) 4'x12'x8' CRANE MATS

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Lifting capacities main boom

Demag AC 180

141,000 lb



360°

85%

Radius ft	Main boom											
	48.2 ft**	48.2 ft	65.6 ft	81.7 ft	98.1 ft	114.8 ft	114.8 ft	131.6 ft	148.0 ft	164.7 ft	181.1 ft	197.0 ft
	1,000 lb											
10	400.0 ¹⁾	338.0	294.0	208.0	-	-	-	-	-	-	-	-
11	375.0 ¹⁾	321.0	290.0	203.0	-	-	-	-	-	-	-	-
13	333.0 ¹⁾	290.0	282.0	195.5	-	-	-	-	-	-	-	-
15	300.0 ¹⁾	264.0	263.0	185.0	148.5	-	-	-	-	-	-	-
16	285.0 ¹⁾	253.0	251.0	180.0	143.5	-	-	-	-	-	-	-
19	241.0	224.0	224.0	167.0	135.0	125.5	109.0	-	-	-	-	-
23	198.0	193.5	192.0	150.5	124.0	111.0	101.0	98.0	-	-	-	-
26	175.5	175.5	174.0	140.5	117.0	102.0	96.0	91.5	83.0	-	-	-
29	159.0	159.0	159.0	131.5	110.0	94.5	91.0	85.5	78.0	64.5	-	-
33	142.0	142.0	141.0	120.5	102.0	85.5	85.5	79.0	71.0	61.5	50.5	39.6
39	-	-	118.0	105.5	91.0	74.5	76.5	68.5	64.0	56.7	46.5	38.8
46	-	-	95.5	92.0	80.0	63.5	68.0	60.0	56.1	51.5	42.5	37.6
52	-	-	82.5	81.0	72.0	56.5	62.0	53.2	50.3	47.3	39.4	36.0
59	-	-	-	68.0	65.0	49.6	56.0	46.7	44.5	42.8	36.1	33.3
65	-	-	-	59.1	59.8	44.6	51.4	42.3	40.5	39.1	33.7	30.8
72	-	-	-	-	51.8	39.8	47.0	38.0	36.4	35.5	31.1	28.0
79	-	-	-	-	44.5	35.8	43.3	34.0	32.9	32.2	29.0	25.7
85	-	-	-	-	39.4	32.7	40.6	31.2	30.1	29.6	27.2	23.6
92	-	-	-	-	-	29.7	36.7	28.1	27.2	27.0	25.3	21.5
98	-	-	-	-	-	27.7	33.1	25.9	25.2	25.0	23.9	20.1
105	-	-	-	-	-	-	-	23.5	22.9	22.9	22.2	18.2
111	-	-	-	-	-	-	-	21.9	21.3	21.3	20.8	17.0
118	-	-	-	-	-	-	-	-	19.4	19.4	19.4	15.6
124	-	-	-	-	-	-	-	-	18.0	18.2	18.0	14.6
131	-	-	-	-	-	-	-	-	16.1	16.8	16.7	13.4
138	-	-	-	-	-	-	-	-	-	15.3	15.3	12.5
144	-	-	-	-	-	-	-	-	-	14.3	14.3	11.7
151	-	-	-	-	-	-	-	-	-	-	13.4	10.7
157	-	-	-	-	-	-	-	-	-	-	12.6	9.9
164	-	-	-	-	-	-	-	-	-	-	11.4	9.2
170	-	-	-	-	-	-	-	-	-	-	-	8.4
177	-	-	-	-	-	-	-	-	-	-	-	7.5

Boom extension sequence in %

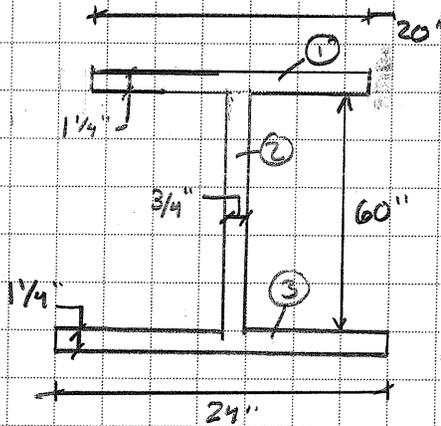
Tele 1	0	0	23	45	45	90	45	90	90	90	90	100
Tele 2	0	0	23	45	45	90	45	90	90	90	90	100
Tele 3	0	0	0	0	45	0	45	45	90	90	90	100
Tele 4	0	0	0	0	0	0	45	0	0	45	90	100

Remarks

- ** special equipment required
- 1) only 0° over rear

CRANE MAT CALCS FOR GIRDER PICK UPS

CROSS SECTION 1



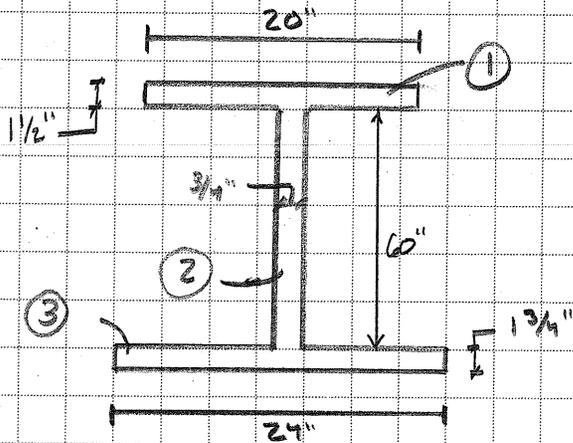
AREA
 1). $(1\frac{1}{4}")(20")$
 2). $(\frac{3}{4}")(60")$
 3). $(1\frac{1}{4}")(24")$
 $\Sigma 100 \text{ in}^2$

DENSITY OF STL:
 $.284 \text{ lb/in}^3$

DEAD LOAD:
 $= 100 \text{ in}^2 \cdot .284 \text{ lb/in}^3$
 $= 28.40 \text{ lb/in}$
 $= 340.80 \text{ plf}$

FACTOR LOAD UP BY 10% = 375 plf

CROSS SECTION 2



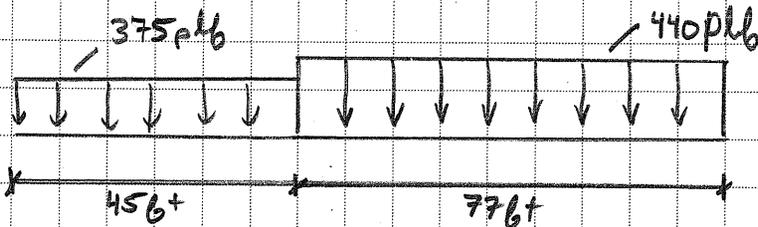
AREA
 1). $(20")(1\frac{1}{2}')$
 2). $(60")(3/4")$
 3). $(24")(1\frac{3}{4}')$
 $\Sigma 117 \text{ in}^2$

DENSITY OF STL
 $.284 \text{ lb/in}^3$

DEAD LOAD:
 $= 117 \text{ in}^2 \cdot .284 \text{ lb/in}^3$
 $= 33.28 \text{ lb/in}$
 $= 398.7 \text{ plf}$

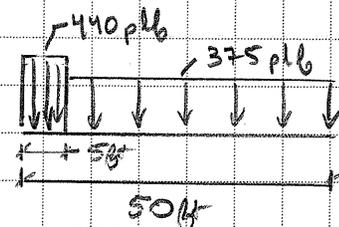
FACTOR LOAD UP BY 10% = 440 plf

GIRDER A



WEIGHT = $440(77) + 375(45)$
 $= 50,755 \text{ lbs}$

GIRDER B



WEIGHT = $(440)(5) + 375(45)$
 $= 19,075 \text{ lbs}$

BEAMBOY V2.0 REPORT

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HL-150T SUPPORT REACTIONS

LOAD CONFIGURATION

Point Loads

6000 lb., x=69.9 ft.
20800 lb., x=62 ft.
8750 lb., x=59.9 ft.
58800 lb., x=0 ft.

Distributed Loads

Start=1020 lb./ft., x=30.8 ft.; End=1020 lb./ft., x=69.9 ft.
Start=63.5 lb./ft., x=0 ft.; End=63.5 lb./ft., x=30.8 ft.

Moments

Supports

Simple support; 30.8 ft., Reaction=134000 lb.
Simple support; 69.9 ft., Reaction=2140 lb.

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DEMAG AC180 SUPPORT REACTIONS

LOAD CONFIGURATION

Point Loads

70500 lb., x=78.2 ft.
63600 lb., x=0 ft.

Distributed Loads

Start=1690 lb./ft., x=39 ft.; End=1690 lb./ft., x=78.2 ft.
Start=150 lb./ft., x=0 ft.; End=150 lb./ft., x=39 ft.

Moments

Supports

Simple support; 39 ft., Reaction=169000 lb.
Simple support; 78.2 ft., Reaction=37400 lb.

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